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Reading: FPE, Sections 3.5–3.6

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= $H_{1}(s) + \frac{1}{a}H_{d}(s), \qquad H_{d}(s) = sH_{1}(s)$

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Step response:

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$$y_2(t) = \mathscr{L}^{-1}\{Y_2(s)\} = \mathscr{L}^{-1}\left\{Y_1(s) + \frac{1}{a} \cdot sY_1(s)\right\} = y_1(t) + \frac{1}{a}\dot{y}_1(t)$$

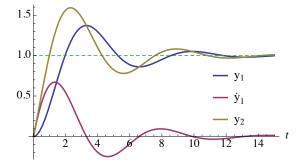
(assuming zero initial conditions)

Step response (zero at s = -a)

$$y_2(t) = y_1(t) + \frac{1}{a}\dot{y}_1(t)$$
 where $y_1(t)$ = original step response

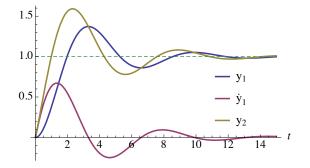
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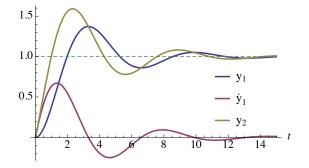


Effects of a LHP zero:

- increased overshoot (major effect)
- ▶ little influence on settling time
- what happens as $a \to \infty$?

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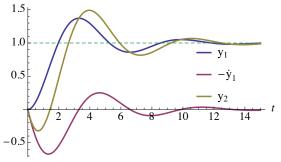
- increased overshoot (major effect)
- ▶ little influence on settling time
- what happens as $a \to \infty$? effects become less significant

What About a RHP Zero?

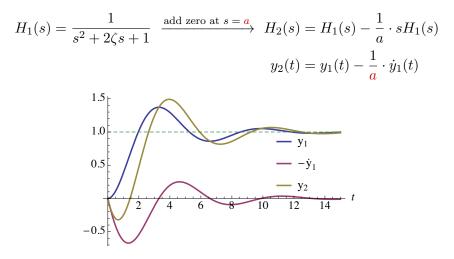
$$H_1(s) = \frac{1}{s^2 + 2\zeta s + 1} \xrightarrow{\text{add zero at } s = a} H_2(s) = H_1(s) - \frac{1}{a} \cdot sH_1(s)$$
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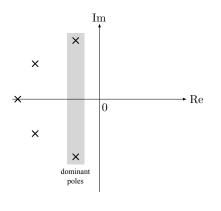


Effects of a RHP zero:

- ▶ slows down (delays) the response
- creates *undershoot* (at least, when a is small enough)

Effect of Extra Poles

A general nth-order system has n poles



- extra LHP poles are not significant if their real parts are at least 5× the real parts of dominant LHP poles
- e.g., if dominant poles have $\operatorname{Re}(s) = -2$ and we have extra poles with $\operatorname{Re}(s) = -10$, their time-domain contributions will be e^{-2t} and $e^{-10t} \ll e^{-2t}$
- ► 5× is just a convention, but we can really see the effect of extra poles that are closer (cf. Lab 2)

Effect of Pole Locations Im × × • Re × × 0 × X

- ▶ poles in open LHP $(\operatorname{Re}(s) < 0)$ stable response
- ▶ poles in open RHP $(\operatorname{Re}(s) > 0)$ unstable response
- ▶ poles on the imaginary axis $(\operatorname{Re}(s) = 0)$ tricky case

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Systems with poles on the imaginary axis are not stable.

What Is Stability?

$$u \longrightarrow h \longrightarrow y$$

One reasonable definition is as follows:

A linear time-invariant system is *Bounded-Input*, *Bounded-Output* (BIBO) *stable* provided either one of the following three equivalent conditions is satisfied:

- 1. If every bounded input u(t) results in a bounded output y(t), regardless of initial conditions.
- 2. If the impulse response h(t) is absolutely integrable:

$$\int_{-\infty}^{\infty} |h(t)| \, \mathrm{d}t < \infty.$$

3. If all poles of the transfer function H(s) are strictly stable (lie in open LHP).

Checking for Stability?

Consider a general transfer function:

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But: often we *don't need to know* precise pole locations, just need to know that they are strictly stable.

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Problem: given an nth-degree polynomial

$$p(s) = s^{n} + a_{1}s^{n-1} + a_{2}s^{n-2} + \ldots + a_{n-1}s + a_{n}$$

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Proof: suppose that p has roots at r_1, r_2, \ldots, r_n with $\operatorname{Re}(r_i) < 0$ for all i. Then

$$p(s) = (s - r_1)(s - r_2) \dots (s - r_n)$$

— multiply this out and check that all coefficients are positive.

Routh–Hurwitz Criterion Necessary & Sufficient Condition for Stability

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We will now introduce a necessary and sufficient condition for stability: the *Routh–Hurwitz Criterion*.

Routh–Hurwitz Criterion: A Bit of History

J.C. Maxwell, "On governors," Proc. Royal Society, no. 100, 1868

... [Stability of the governor] is mathematically equivalent to the condition that all the possible roots, and all the possible parts of the impossible roots, of a certain equation shall be negative. ... I have not been able completely to determine these conditions for equations of a higher degree than the third; but I hope that the subject will obtain the attention of mathematicians.



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In 1893, Adolf Hurwitz solved the same problem, using a different method, independently of Routh.



Edward John Routh, 1831–1907



Adolf Hurwitz, 1859–1919

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We begin by forming the Routh array using the coefficients of *p*:

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Note that the very first entry is always 1, and also note the order in which the coefficients are filled in.

 $s^n: 1 a_2 a_4 a_6 \dots s^{n-1}: a_1 a_3 a_5 a_7 \dots$

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Next, we form the third row marked by s^{n-2} :

$$s^{n-2}$$
: b_1 b_2 b_3 ...

where

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Note: the new row is 1 element shorter than the one above it

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where $c_1 = -\frac{1}{b_1} \det \begin{pmatrix} a_1 & a_3 \\ b_1 & b_2 \end{pmatrix} = -\frac{1}{b_1} (a_1b_2 - a_3b_1)$

$$s^n: 1 \quad a_2 \quad a_4 \quad a_6 \quad \dots \\ s^{n-1}: a_1 \quad a_3 \quad a_5 \quad a_7 \quad \dots \\ s^{n-2}: b_1 \quad b_2 \quad b_3 \quad \dots$$

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and so on \ldots

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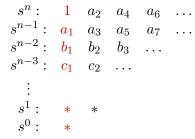
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and so on \ldots

Eventually, we complete the array like this:



(as long as we don't get stuck with

division by zero: more on this later)

Eventually, we complete the array like this:

After the process terminates, we will have n + 1 entries in the first column.

The Routh–Hurwitz Criterion

Consider degree-n polynomial

$$p(s) = s^n + a_1 s^{n-1} + \ldots + a_{n-1} s + a_n$$

and form the Routh array:

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The Routh-Hurwitz criterion: Assume that the necessary condition for stability holds, i.e., $a_1, \ldots, a_n > 0$. Then:

- ▶ p is stable if and only if all entries in the first column are positive;
- otherwise, #(RHP poles) = #(sign changes in 1st column)

Example

Check stability of

$$p(s) = s^4 + 4s^3 + s^2 + 2s + 3$$

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$$s^4: 1 1 3 s^3: 4 2 0$$

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All coefficients strictly positive: necessary condition checks out.

Answer: p is unstable — it has 2 RHP poles (2 sign changes in 1st column)

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— p is stable iff $a_1, a_2 > 0$ (necessary and sufficient).

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— p is stable iff $a_1, a_2, a_3 > 0$ (necc. cond.) and $a_1a_2 > a_3$

Stability Conditions for Low-Order Polynomials

The upshot:

- ► A 2nd-degree polynomial $p(s) = s^2 + a_1s + a_2$ is stable if and only if $a_1 > 0$ and $a_2 > 0$
- ► A 3rd-degree polynomial $p(s) = s^3 + a_1s^2 + a_2s + a_3$ is stable if and only if $a_1, a_2, a_3 > 0$ and $a_1a_2 > a_3$

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- These conditions were already obtained by Maxwell in 1868.
- ▶ In both cases, the computations were *purely symbolic*: this can make a lot of difference in *design*, as opposed to *analysis*.

Routh–Hurwitz as a Design Tool

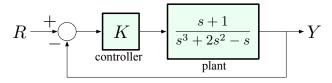
Parametric stability range

We can use the Routh test to determine *parameter ranges* for stability.

Routh–Hurwitz as a Design Tool Parametric stability range

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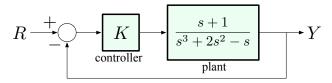
Example: consider the unity feedback configuration



Routh–Hurwitz as a Design Tool Parametric stability range

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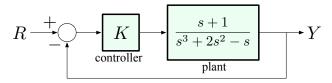


Note that the plant is *unstable* (the denominator has a negative coefficient and a zero coefficient).

Routh–Hurwitz as a Design Tool Parametric stability range

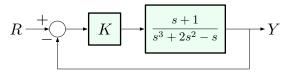
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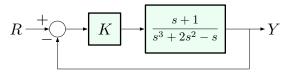


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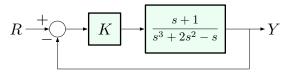
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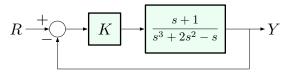
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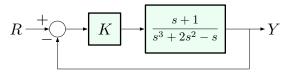
Let's write down the transfer function from R to Y:

 $\frac{Y}{R} = \frac{\text{forward gain}}{1 + \text{loop gain}}$



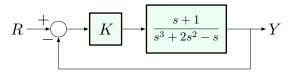
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$$R \xrightarrow{+} K \xrightarrow{s+1} Y$$

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Now we need to test stability of $p(s) = s^3 + 2s^2 + (K-1)s + K$.

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$$\frac{K}{2} - 1 > 0 \quad \text{and} \quad K > 0$$

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Note: The necessary condition requires K > 1, but now we actually know that we must have K > 2 for stability.

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- ▶ For an *entire row of zeros*, the procedure is a more complicated (see Example 3.34 in FPE) we will not worry about this too much.