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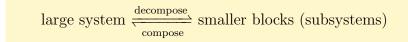
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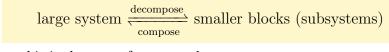
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Reading: FPE, Sections 3.1–3.2; lab manual

System Modeling Diagrams

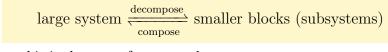


System Modeling Diagrams



— this is the core of systems theory

System Modeling Diagrams

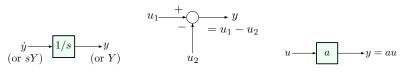


— this is the core of systems theory

We will take smaller blocks from some given *library* and play with them to create/build more complicated systems.

All-Integrator Diagrams

Our library will consist of three building blocks:



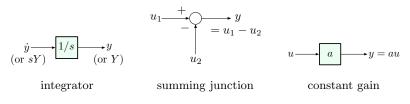
integrator

summing junction

constant gain

All-Integrator Diagrams

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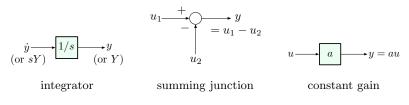


Two warnings:

- ► We can (and will) work either with u, y (time domain) or with U, Y (s-domain) — will often go back and forth
- ▶ When working with block diagrams, we typically ignore initial conditions.

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This is the *lowest level* we will go to in lectures; in the labs, you will implement these blocks using op amps.

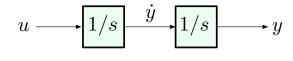
Build an all-integrator diagram for

$$\ddot{y} = u \qquad \Longleftrightarrow \qquad s^2 Y = U$$

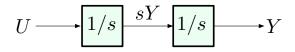
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This is obvious:



or



(building on Example 1)

$$\ddot{y} + a_1 \dot{y} + a_0 y = u \qquad \Longleftrightarrow \qquad s^2 Y + a_1 s Y + a_0 Y = U$$

or $Y(s) = \frac{U(s)}{s^2 + a_1 s + a_0}$

Example 2 (building on Example 1)

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Always solve for the highest derivative:

$$\ddot{y} = \underbrace{-a_1\dot{y} - a_0y + u}_{=v}$$

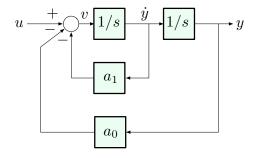
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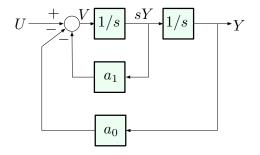
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Note: $b_0 + b_1 s$ involves *differentiation*, which we cannot implement using an all-integrator diagram. But we will see that we don't need to do it directly.

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Example 3, continued Step 1: decompose $H(s) = \frac{1}{s^2 + a_1s + a_0} \cdot (b_1s + b_0)$

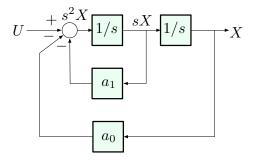
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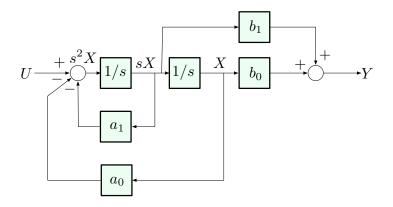
$$Y(s) = b_1 s X(s) + b_0 X(s),$$

and both X and sX are available signals in our diagram. So:

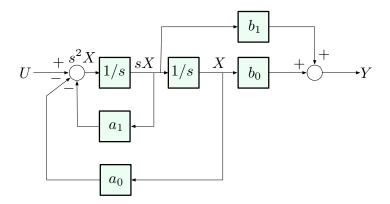
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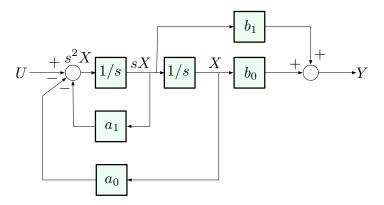
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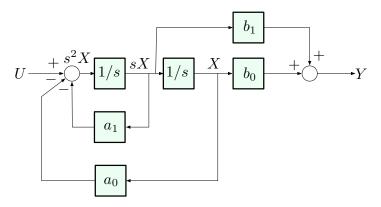
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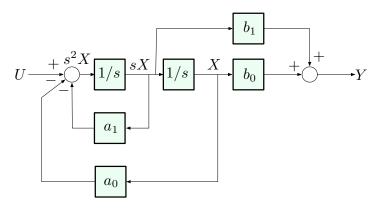


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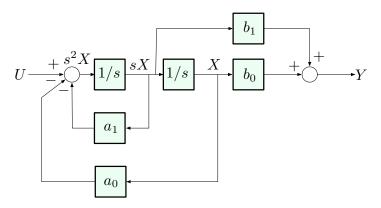


Can we write down a state-space model corresponding to this diagram?

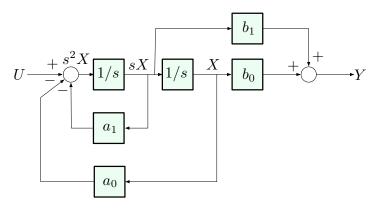




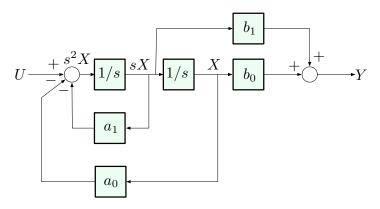
$$s^2 X = U - a_1 s X - a_0 X$$



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This is called *controller canonical form*.

Example 3, continued

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- Easily generalizes to dimension > 1
- ▶ The reason behind the name will be made clear later in the semester

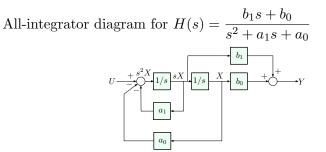
Example 3, wrap-up

All-integrator diagram for $H(s) = \frac{b_1 s + b_0}{s^2 + a_1 s + a_0}$ $U \xrightarrow{+s^2 X} 1/s \xrightarrow{sX} 1/s \xrightarrow{b_1} + b_0 \xrightarrow{++} Y$

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Important: for a given H(s), the diagram is not unique. But, once we build a diagram, the state-space equations are unique (up to coordinate transformations).

Now we will take this a level higher — we will talk about building complex systems from smaller blocks, without worrying about how those blocks look on the inside (they could themselves be all-integrator diagrams, etc.)

Basic System Interconnections

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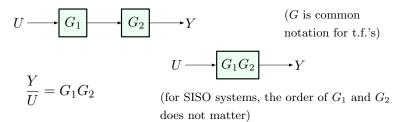
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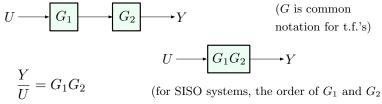
Block diagrams describe the *flow of information*

Basic System Interconnections: Series & Parallel



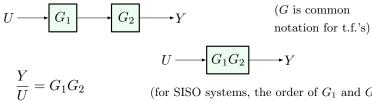
(G is common notation for t.f.'s)



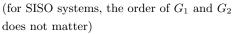


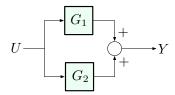
Parallel connection

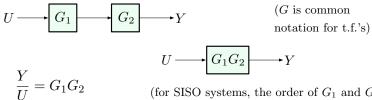
does not matter)



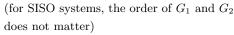
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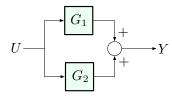




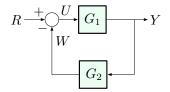


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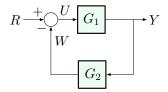




 $\frac{Y}{U} = G_1 + G_2 \qquad \qquad U \longrightarrow G_1 + G_2 \longrightarrow Y$

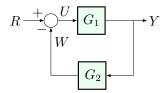


Find the transfer function from R (reference) to Y



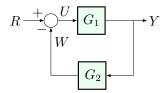
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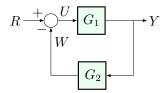
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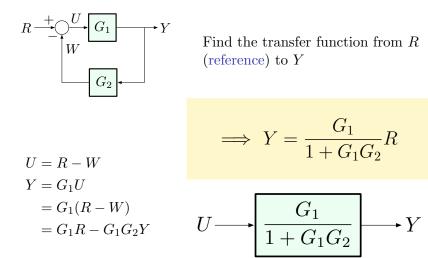
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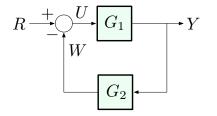
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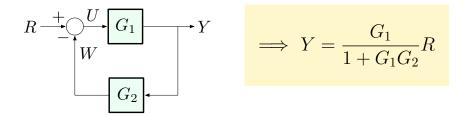
$$= G_1 (R - W)$$

$$= G_1 R - G_1 G_2 Y$$



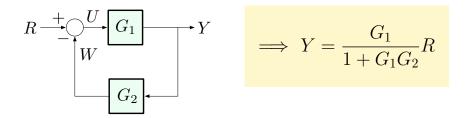


 $\implies Y = \frac{G_1}{1 + G_1 G_2} R$



The gain of a negative feedback loop:

 $\frac{\text{forward gain}}{1 + \text{loop gain}}$



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This is an important relationship, easy to derive — no need to memorize it.

Other feedback configurations are also possible:

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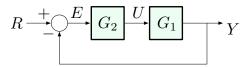
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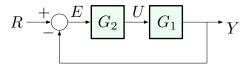
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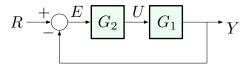
Common structure (saw this in Lecture 1):

- $\blacktriangleright R = reference$
- U = control input
- Y = output
- $\blacktriangleright E = \text{error}$
- $G_1 = \text{plant}$ (also denoted by P)
- $G_2 = \text{controller or compensator (also denoted by C or K)}$





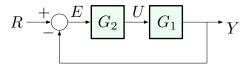
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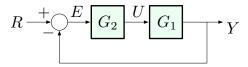


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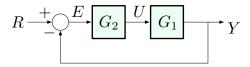
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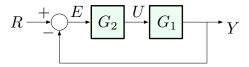
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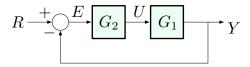
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• Error E to output Y:

$$\frac{Y}{E} = G_1 G_2 \qquad \text{(no feedback path)}$$

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This requires lots of practice: read FPE, Section 3.2 for examples.

General strategy:

- ▶ Name all the variables in the diagram
- Write down as many relationships between these variables as you can
- ▶ Learn to recognize series, parallel, and feedback interconnections
- ▶ Replace them by their equivalents
- Repeat

So far, we have only seen transfer functions that have either real poles or purely imaginary poles:

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Plus, you will need this for Lab 1.

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- ▶ H(s) is normalized to have DC gain = 1 (provided DC gain exists)

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The nature of the poles changes depending on ζ :

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$$-\sigma \pm j\omega_d$$

where $\sigma = \zeta \omega_n, \ \omega_d = \omega_n \sqrt{1 - \zeta^2}$

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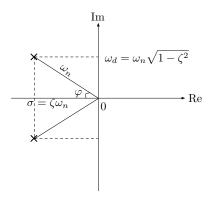
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Note that

$$\sigma^{2} + \omega_{d}^{2} = \zeta^{2}\omega_{n}^{2} + \omega_{n}^{2} - \zeta^{2}\omega_{n}^{2}$$
$$= \omega_{n}^{2}$$
$$\cos\varphi = \frac{\zeta\omega_{n}}{\omega_{n}} = \zeta$$

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2nd-Order Step Response

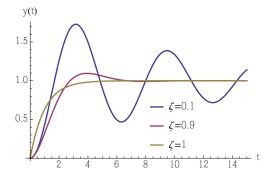
$$H(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} = \frac{\omega_n^2}{(s+\sigma)^2 + \omega_d^2}$$
$$u(t) = 1(t) \qquad \longrightarrow \qquad y(t) = 1 - e^{-\sigma t} \left(\cos(\omega_d t) + \frac{\sigma}{\omega_d}\sin(\omega_d t)\right)$$

where $\sigma = \zeta \omega_n$ and $\omega_d = \omega_n \sqrt{1 - \zeta^2}$ (damped frequency)

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The parameter ζ is called the *damping ratio*

- $\zeta > 1$: system is overdamped
- $\zeta < 1$: system is underdamped
- $\zeta = 0$: no damping $(\omega_d = \omega_n)$