Plan of the Lecture

- ▶ Review: control, feedback, etc.
- ▶ Today's topic: state-space models of systems; linearization

Plan of the Lecture

- ▶ Review: control, feedback, etc.
- ▶ Today's topic: state-space models of systems; linearization

Goal: a general framework that encompasses all examples of interest. Once we have mastered this framework, we can proceed to *analysis* and then to *design*.

Plan of the Lecture

- ▶ Review: control, feedback, etc.
- ▶ Today's topic: state-space models of systems; linearization

Goal: a general framework that encompasses all examples of interest. Once we have mastered this framework, we can proceed to *analysis* and then to *design*.

Reading: FPE, Sections 1.1, 1.2, 2.1–2.4, 7.2, 9.2.1. Chapter 2 has lots of cool examples of system models!!

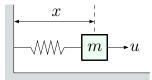
Notation Reminder

We will be looking at *dynamic systems* whose evolution *in time* is described by *differential equations* with *external inputs*.

We will not write the time variable t explicitly, so we use

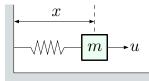
$$\begin{array}{ll} x & \text{instead of} & x(t) \\ \dot{x} & \text{instead of} & x'(t) \text{ or } \frac{\mathrm{d}x}{\mathrm{d}t} \\ \ddot{x} & \text{instead of} & x''(t) \text{ or } \frac{\mathrm{d}^2x}{\mathrm{d}t^2} \end{array}$$

etc.



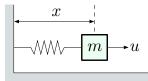
Newton's second law (translational motion):

$$\underbrace{F}_{\text{total force}} = ma$$



Newton's second law (translational motion):

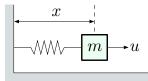
$$F_{\text{total force}} = ma = \text{spring force} + \text{friction} + \text{external force}$$



Newton's second law (translational motion):

 $F_{\text{total force}} = ma = \text{spring force} + \text{friction} + \text{external force}$

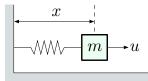
spring force = -kx (Hooke's law) friction force $= -\rho \dot{x}$ (Stokes' law — linear drag, only an approximation!!)



Newton's second law (translational motion):

 $F_{\text{total force}} = ma = \text{spring force} + \text{friction} + \text{external force}$

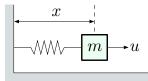
spring force = -kx (Hooke's law) friction force $= -\rho \dot{x}$ (Stokes' law — linear drag, only an approximation!!) $F = -kx - \rho \dot{x} + u$



Newton's second law (translational motion):

 $F_{\text{total force}} = ma = \text{spring force} + \text{friction} + \text{external force}$

spring force = -kx (Hooke's law) friction force $= -\rho \dot{x}$ (Stokes' law — linear drag, only an approximation!!) $m\ddot{x} = -kx - \rho \dot{x} + u$



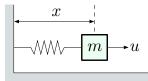
Newton's second law (translational motion):

 $F_{\text{total force}} = ma = \text{spring force} + \text{friction} + \text{external force}$

spring force = -kx (Hooke's law) friction force $= -\rho \dot{x}$ (Stokes' law — linear drag, only an approximation!!) $m\ddot{x} = -kx - \rho \dot{x} + u$

Move x, \dot{x}, \ddot{x} to the LHS, u to the RHS:

$$m\ddot{x} + \rho\dot{x} + kx = u$$



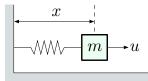
Newton's second law (translational motion):

 $F_{\text{total force}} = ma = \text{spring force} + \text{friction} + \text{external force}$

spring force = -kx (Hooke's law) friction force $= -\rho \dot{x}$ (Stokes' law — linear drag, only an approximation!!) $m\ddot{x} = -kx - \rho \dot{x} + u$

Move x, \dot{x}, \ddot{x} to the LHS, u to the RHS:

$$\ddot{x} + \frac{\rho}{m}\dot{x} + \frac{k}{m}x = \frac{u}{m}$$



Newton's second law (translational motion):

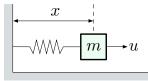
 $F_{\text{total force}} = ma = \text{spring force} + \text{friction} + \text{external force}$

spring force = -kx (Hooke's law) friction force $= -\rho \dot{x}$ (Stokes' law — linear drag, only an approximation!!) $m\ddot{x} = -kx - \rho \dot{x} + u$

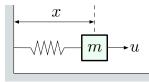
Move x, \dot{x}, \ddot{x} to the LHS, u to the RHS:

$$\ddot{x} + \frac{\rho}{m}\dot{x} + \frac{k}{m}x = \frac{u}{m}$$

2nd-order linear ODE

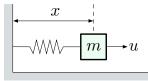


$$\ddot{x} + \frac{\rho}{m}\dot{x} + \frac{k}{m}x = \frac{u}{m}$$
 2nd-order linear ODE



$$\ddot{x} + \frac{\rho}{m}\dot{x} + \frac{k}{m}x = \frac{u}{m}$$
 2nd-order linear ODE

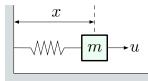
Canonical form: convert to a system of 1st-order ODEs



$$\ddot{x} + \frac{\rho}{m}\dot{x} + \frac{k}{m}x = \frac{u}{m}$$
 2nd-order linear ODE

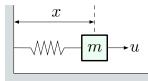
Canonical form: convert to a system of 1st-order ODEs

$$\dot{x} = v$$
 (definition of velocity
 $\dot{v} = -\frac{\rho}{m}v - \frac{k}{m}x + \frac{1}{m}u$



State-space model: express in *matrix form*

$$\begin{pmatrix} \dot{x} \\ \dot{v} \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{\rho}{m} \end{pmatrix} \begin{pmatrix} x \\ v \end{pmatrix} + \begin{pmatrix} 0 \\ \frac{1}{m} \end{pmatrix} u$$



State-space model: express in matrix form

$$\begin{pmatrix} \dot{x} \\ \dot{v} \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{\rho}{m} \end{pmatrix} \begin{pmatrix} x \\ v \end{pmatrix} + \begin{pmatrix} 0 \\ \frac{1}{m} \end{pmatrix} u$$

Important: start reviewing your linear algebra *now*!!

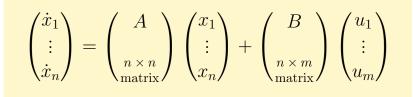
▶ matrix-vector multiplication; eigenvalues and eigenvectors; etc.

General n-Dimensional State-Space Model

state
$$x = \begin{pmatrix} x_1 \\ \vdots \\ x_n \end{pmatrix} \in \mathbb{R}^n$$
 input $u = \begin{pmatrix} u_1 \\ \vdots \\ u_m \end{pmatrix} \in \mathbb{R}^m$

General *n*-Dimensional State-Space Model

state
$$x = \begin{pmatrix} x_1 \\ \vdots \\ x_n \end{pmatrix} \in \mathbb{R}^n$$
 input $u = \begin{pmatrix} u_1 \\ \vdots \\ u_m \end{pmatrix} \in \mathbb{R}^m$



General n-Dimensional State-Space Model

state
$$x = \begin{pmatrix} x_1 \\ \vdots \\ x_n \end{pmatrix} \in \mathbb{R}^n$$
 input $u = \begin{pmatrix} u_1 \\ \vdots \\ u_m \end{pmatrix} \in \mathbb{R}^m$

$$\begin{pmatrix} \dot{x}_1 \\ \vdots \\ \dot{x}_n \end{pmatrix} = \begin{pmatrix} A \\ \\ \\ n \times n \\ matrix \end{pmatrix} \begin{pmatrix} x_1 \\ \vdots \\ x_n \end{pmatrix} + \begin{pmatrix} B \\ \\ \\ \\ matrix \end{pmatrix} \begin{pmatrix} u_1 \\ \vdots \\ u_m \end{pmatrix}$$

$$\dot{x} = Ax + Bu$$

state
$$x = \begin{pmatrix} x_1 \\ \vdots \\ x_n \end{pmatrix} \in \mathbb{R}^n$$
 input $u = \begin{pmatrix} u_1 \\ \vdots \\ u_m \end{pmatrix} \in \mathbb{R}^m$

state
$$x = \begin{pmatrix} x_1 \\ \vdots \\ x_n \end{pmatrix} \in \mathbb{R}^n$$
 input $u = \begin{pmatrix} u_1 \\ \vdots \\ u_m \end{pmatrix} \in \mathbb{R}^m$
output $y = \begin{pmatrix} y_1 \\ \vdots \\ y_p \end{pmatrix} \in \mathbb{R}^p$ $y = Cx$ $C - p \times n$ matrix

state
$$x = \begin{pmatrix} x_1 \\ \vdots \\ x_n \end{pmatrix} \in \mathbb{R}^n$$
 input $u = \begin{pmatrix} u_1 \\ \vdots \\ u_m \end{pmatrix} \in \mathbb{R}^m$
output $y = \begin{pmatrix} y_1 \\ \vdots \\ y_p \end{pmatrix} \in \mathbb{R}^p$ $y = Cx$ $C - p \times n$ matrix

$$\dot{x} = Ax + Bu$$
$$y = Cx$$

state
$$x = \begin{pmatrix} x_1 \\ \vdots \\ x_n \end{pmatrix} \in \mathbb{R}^n$$
 input $u = \begin{pmatrix} u_1 \\ \vdots \\ u_m \end{pmatrix} \in \mathbb{R}^m$
output $y = \begin{pmatrix} y_1 \\ \vdots \\ y_p \end{pmatrix} \in \mathbb{R}^p$ $y = Cx$ $C - p \times n$ matrix

$$\dot{x} = Ax + Bu$$
$$y = Cx$$

Example: if we only care about (or can only measure) x_1 , then

$$y = x_1 = \begin{pmatrix} 1 & 0 & \dots & 0 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{pmatrix}$$

$$\dot{x} = Ax + Bu$$
$$y = Cx$$

$$\dot{x} = Ax + Bu$$
$$y = Cx$$

State-space models are useful and convenient for writing down system models for different types of systems, in a unified manner.

$$\dot{x} = Ax + Bu$$
$$y = Cx$$

State-space models are useful and convenient for writing down system models for different types of systems, in a unified manner.

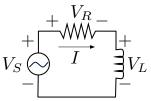
When working with state-space models, what are *states* and what are *inputs*?

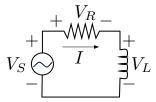
$$\dot{x} = Ax + Bu$$
$$y = Cx$$

State-space models are useful and convenient for writing down system models for different types of systems, in a unified manner.

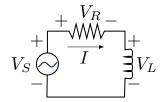
When working with state-space models, what are *states* and what are *inputs*?

— match against $\dot{x} = Ax + Bu$



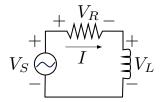


$$-V_S + V_R + V_L = 0$$
 Kirchhoff's voltage law
 $V_R = RI$ Ohm's law
 $V_L = L\dot{I}$ Faraday's law
 $-V_S + RI + L\dot{I} = 0$



 $-V_S + V_R + V_L = 0$ Kirchhoff's voltage law $V_R = RI$ Ohm's law $V_L = L\dot{I}$ Faraday's law $-V_S + RI + L\dot{I} = 0$

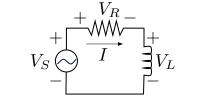
$$\dot{I} = -\frac{R}{L}I + \frac{1}{L}V_S \qquad (\text{1st-order system})$$



 $-V_S + V_R + V_L = 0$ Kirchhoff's voltage law $V_R = RI$ Ohm's law $V_L = L\dot{I}$ Faraday's law $-V_S + RI + L\dot{I} = 0$

$$\dot{I} = -\frac{R}{L}I + \frac{1}{L}V_S \qquad (\text{1st-order system})$$

 $I - \text{state}, V_S - \text{input}$

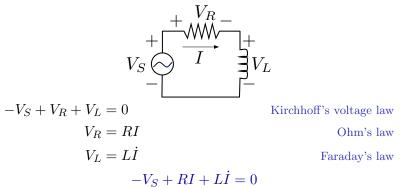


 $-V_S + V_R + V_L = 0$ Kirchhoff's voltage law $V_R = RI$ Ohm's law $V_L = L\dot{I}$ Faraday's law $-V_S + RI + L\dot{I} = 0$

$$\dot{I} = -\frac{R}{L}I + \frac{1}{L}V_S \qquad ({\rm 1st-order\ system})$$

I – state, V_S – input

Q: How should we change the circuit in order to implement a 2nd-order system?

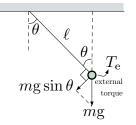


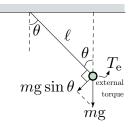
$$\dot{I} = -\frac{R}{L}I + \frac{1}{L}V_S \qquad ({\rm 1st-order\ system})$$

I – state, V_S – input

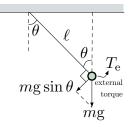
Q: How should we change the circuit in order to implement a 2nd-order system? A: Add a capacitor.

Example 3: Pendulum





Newton's 2nd law (rotational motion):



Newton's 2nd law (rotational motion):

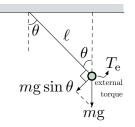
 α

total

torque

moment

angular of inertia acceleration



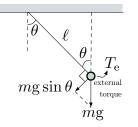
Newton's 2nd law (rotational motion):

 α

total torque

moment angular of inertia acceleration

= pendulum torque + external torque



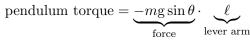
Newton's 2nd law (rotational motion):

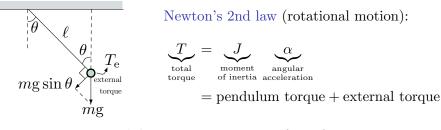


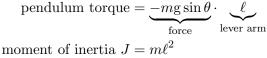
total torque

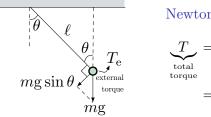
moment angular of inertia acceleration

= pendulum torque + external torque







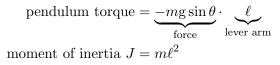


Newton's 2nd law (rotational motion):

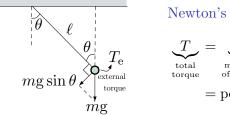


moment angular of inertia acceleration

= pendulum torque + external torque



$$-mg\ell\sin\theta + T_e = m\ell^2\ddot{\theta}$$



Newton's 2nd law (rotational motion):



moment angular of inertia acceleration

= pendulum torque + external torque

pendulum torque =
$$\underbrace{-mg\sin\theta}_{\text{force}} \cdot \underbrace{\ell}_{\text{lever arm}}$$

moment of inertia $J = m\ell^2$

$$-mg\ell\sin\theta + T_{\rm e} = m\ell^2\ddot{\theta}$$

$$\ddot{\theta} = -\frac{\mathrm{g}}{\ell}\sin\theta + \frac{1}{m\ell^2}T_{\mathrm{e}}$$

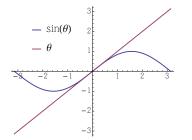
(nonlinear equation)

$$\ddot{\theta} = -\frac{g}{\ell}\sin\theta + \frac{1}{m\ell^2}T_e$$

(nonlinear equation)

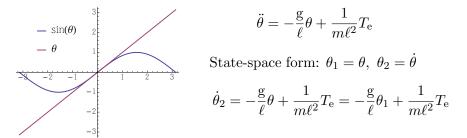
$$\ddot{\theta} = -\frac{g}{\ell}\sin\theta + \frac{1}{m\ell^2}T_e$$
 (nonlinear equation)

$$\ddot{\theta} = -\frac{g}{\ell}\sin\theta + \frac{1}{m\ell^2}T_e$$
 (nonlinear equation)

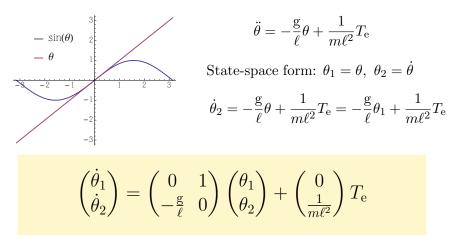


$$\ddot{\theta} = -\frac{\mathrm{g}}{\ell}\theta + \frac{1}{m\ell^2}T_{\mathrm{e}}$$

$$\ddot{\theta} = -\frac{g}{\ell}\sin\theta + \frac{1}{m\ell^2}T_e$$
 (nonlinear equation)



$$\ddot{\theta} = -\frac{g}{\ell}\sin\theta + \frac{1}{m\ell^2}T_e$$
 (nonlinear equation)



Taylor series expansion:

$$f(x) = f(x_0) + f'(x_0)(x - x_0) + \frac{1}{2}f''(x_0)(x - x_0)^2 + \dots$$

$$\approx f(x_0) + f'(x_0)(x - x_0) \qquad \text{linear approximation around } x = x_0$$

Taylor series expansion:

$$f(x) = f(x_0) + f'(x_0)(x - x_0) + \frac{1}{2}f''(x_0)(x - x_0)^2 + \dots$$

$$\approx f(x_0) + f'(x_0)(x - x_0) \qquad \text{linear approximation around } x = x_0$$

Control systems are generally *nonlinear*:

$$\dot{x} = f(x, u) \qquad \text{nonlinear state-space model}$$
$$x = \begin{pmatrix} x_1 \\ \vdots \\ x_n \end{pmatrix} \quad u = \begin{pmatrix} u_1 \\ \vdots \\ u_m \end{pmatrix} \quad f = \begin{pmatrix} f_1 \\ \vdots \\ f_n \end{pmatrix}$$

Taylor series expansion:

$$f(x) = f(x_0) + f'(x_0)(x - x_0) + \frac{1}{2}f''(x_0)(x - x_0)^2 + \dots$$

$$\approx f(x_0) + f'(x_0)(x - x_0) \qquad \text{linear approximation around } x = x_0$$

Control systems are generally *nonlinear*:

$$\dot{x} = f(x, u) \qquad \text{nonlinear state-space model}$$
$$x = \begin{pmatrix} x_1 \\ \vdots \\ x_n \end{pmatrix} \quad u = \begin{pmatrix} u_1 \\ \vdots \\ u_m \end{pmatrix} \quad f = \begin{pmatrix} f_1 \\ \vdots \\ f_n \end{pmatrix}$$

Assume x = 0, u = 0 is an *equilibrium point*: f(0, 0) = 0

This means that, when the system is at rest and no control is applied, the system does not move.

Linear approx. around (x, u) = (0, 0) to all components of f:

$$\dot{x}_1 = f_1(x, u), \qquad \dots, \qquad \dot{x}_n = f_n(x, u)$$

Linear approx. around (x, u) = (0, 0) to all components of f:

$$\dot{x}_1 = f_1(x, u), \qquad \dots, \qquad \dot{x}_n = f_n(x, u)$$

For each $i = 1, \ldots, n$,

$$f_i(x,u) = \underbrace{f_i(0,0)}_{=0} + \frac{\partial f_i}{\partial x_1}(0,0)x_1 + \dots + \frac{\partial f_i}{\partial x_n}(0,0)x_n + \frac{\partial f_i}{\partial u_1}(0,0)u_1 + \dots + \frac{\partial f_i}{\partial u_m}(0,0)u_m$$

Linear approx. around (x, u) = (0, 0) to all components of f:

$$\dot{x}_1 = f_1(x, u), \qquad \dots, \qquad \dot{x}_n = f_n(x, u)$$

For each $i = 1, \ldots, n$,

$$f_i(x,u) = \underbrace{f_i(0,0)}_{=0} + \frac{\partial f_i}{\partial x_1}(0,0)x_1 + \ldots + \frac{\partial f_i}{\partial x_n}(0,0)x_n + \frac{\partial f_i}{\partial u_1}(0,0)u_1 + \ldots + \frac{\partial f_i}{\partial u_m}(0,0)u_m$$

Linearized state-space model:

$$\dot{x} = Ax + Bu$$
, where $A_{ij} = \frac{\partial f_i}{\partial x_j}\Big|_{x=0 \atop u=0}$, $B_{ik} = \frac{\partial f_i}{\partial u_k}\Big|_{x=0 \atop u=0}$

Linear approx. around (x, u) = (0, 0) to all components of f:

$$\dot{x}_1 = f_1(x, u), \qquad \dots, \qquad \dot{x}_n = f_n(x, u)$$

For each $i = 1, \ldots, n$,

$$f_i(x,u) = \underbrace{f_i(0,0)}_{=0} + \frac{\partial f_i}{\partial x_1}(0,0)x_1 + \ldots + \frac{\partial f_i}{\partial x_n}(0,0)x_n + \frac{\partial f_i}{\partial u_1}(0,0)u_1 + \ldots + \frac{\partial f_i}{\partial u_m}(0,0)u_m$$

Linearized state-space model:

$$\dot{x} = Ax + Bu$$
, where $A_{ij} = \frac{\partial f_i}{\partial x_j}\Big|_{x=0\atop u=0}$, $B_{ik} = \frac{\partial f_i}{\partial u_k}\Big|_{x=0\atop u=0}$

Important: since we have ignored the higher-order terms, this linear system is only an *approximation* that holds only for *small deviations* from equilibrium.

Example 3: Pendulum, Revisited

Original nonlinear state-space model:

$$\dot{ heta}_1 = f_1(heta_1, heta_2, T_{
m e}) = heta_2$$
 — already linear
 $\dot{ heta}_2 = f_2(heta_1, heta_2, T_{
m e}) = -rac{{
m g}}{\ell}\sin heta_1 + rac{1}{m\ell^2}T_{
m e}$

Example 3: Pendulum, Revisited

Original nonlinear state-space model:

$$\begin{split} \dot{\theta}_1 &= f_1(\theta_1, \theta_2, T_{\rm e}) = \theta_2 \qquad - \text{ already linear} \\ \dot{\theta}_2 &= f_2(\theta_1, \theta_2, T_{\rm e}) = -\frac{\text{g}}{\ell} \sin \theta_1 + \frac{1}{m\ell^2} T_{\rm e} \end{split}$$

Linear approx. of f_2 around equilibrium $(\theta_1, \theta_2, T_e) = (0, 0, 0)$:

$$\frac{\partial f_2}{\partial \theta_1} = -\frac{g}{\ell} \cos \theta_1 \qquad \frac{\partial f_2}{\partial \theta_2} = 0 \qquad \frac{\partial f_2}{\partial T_e} = \frac{1}{m\ell^2}$$
$$\frac{\partial f_2}{\partial \theta_1} \bigg|_0 = -\frac{g}{\ell} \qquad \frac{\partial f_2}{\partial \theta_2} \bigg|_0 = 0 \qquad \frac{\partial f_2}{\partial T_e} \bigg|_0 = \frac{1}{m\ell^2}$$

Example 3: Pendulum, Revisited

Original nonlinear state-space model:

$$\dot{\theta}_1 = f_1(\theta_1, \theta_2, T_e) = \theta_2$$
 — already linear
 $\dot{\theta}_2 = f_2(\theta_1, \theta_2, T_e) = -\frac{g}{\ell} \sin \theta_1 + \frac{1}{m\ell^2} T_e$

Linear approx. of f_2 around equilibrium $(\theta_1, \theta_2, T_e) = (0, 0, 0)$:

$$\begin{aligned} \frac{\partial f_2}{\partial \theta_1} &= -\frac{\mathbf{g}}{\ell} \cos \theta_1 \qquad \frac{\partial f_2}{\partial \theta_2} = 0 \qquad \frac{\partial f_2}{\partial T_{\mathbf{e}}} = \frac{1}{m\ell^2} \\ \frac{\partial f_2}{\partial \theta_1} \bigg|_0 &= -\frac{\mathbf{g}}{\ell} \qquad \frac{\partial f_2}{\partial \theta_2} \bigg|_0 = 0 \qquad \frac{\partial f_2}{\partial T_{\mathbf{e}}} \bigg|_0 = \frac{1}{m\ell^2} \end{aligned}$$

Linearized state-space model of the pendulum:

$$\begin{aligned} \theta_1 &= \theta_2 \\ \dot{\theta}_2 &= -\frac{\mathrm{g}}{\ell} \theta_1 + \frac{1}{m\ell^2} T_\mathrm{e} \end{aligned}$$

valid for *small* deviations from equ.

▶ Start from nonlinear state-space model

$$\dot{x} = f(x, u)$$

▶ Start from nonlinear state-space model

$$\dot{x} = f(x, u)$$

Find equilibrium point (x_0, u_0) such that $f(x_0, u_0) = 0$

▶ Start from nonlinear state-space model

$$\dot{x} = f(x, u)$$

Find equilibrium point (x_0, u_0) such that $f(x_0, u_0) = 0$ *Note:* different systems may have different equilibria, not necessarily (0, 0), so we need to shift variables:

$$\underline{x} = x - x_0 \qquad \underline{u} = u - u_0$$

$$\underline{f}(\underline{x}, \underline{u}) = f(\underline{x} + x_0, \underline{u} + u_0) = f(x, u)$$

▶ Start from nonlinear state-space model

$$\dot{x} = f(x, u)$$

Find equilibrium point (x_0, u_0) such that $f(x_0, u_0) = 0$ *Note:* different systems may have different equilibria, not necessarily (0, 0), so we need to shift variables:

$$\underline{x} = x - x_0 \qquad \underline{u} = u - u_0$$

$$\underline{f}(\underline{x}, \underline{u}) = f(\underline{x} + x_0, \underline{u} + u_0) = f(x, u)$$

Note that the transformation is *invertible*:

$$x = \underline{x} + x_0, \qquad u = \underline{u} + u_0$$

• Pass to shifted variables $\underline{x} = x - x_0$, $\underline{u} = u - u_0$

— equivalent to original system

• Pass to shifted variables $\underline{x} = x - x_0$, $\underline{u} = u - u_0$

 $\underline{\dot{x}} = \dot{x} \qquad (x_0 \text{ does not depend on } t)$ = f(x, u) $= \underline{f}(\underline{x}, \underline{u})$

- equivalent to original system
- The transformed system is in equilibrium at (0,0):

$$\underline{f}(0,0) = f(x_0, u_0) = 0$$

▶ Pass to shifted variables $\underline{x} = x - x_0$, $\underline{u} = u - u_0$

$$\underline{\dot{x}} = \dot{x} \qquad (x_0 \text{ does not depend on } t)$$

$$= f(x, u)$$

$$= \underline{f}(\underline{x}, \underline{u})$$

— equivalent to original system

• The transformed system is in equilibrium at (0, 0):

$$\underline{f}(0,0) = f(x_0, u_0) = 0$$

Now linearize:

$$\underline{\dot{x}} = A\underline{x} + B\underline{u}, \quad \text{where } A_{ij} = \frac{\partial f_i}{\partial x_j} \bigg|_{\substack{x=x_0\\u=u_0}}, \ B_{ik} = \frac{\partial f_i}{\partial u_k} \bigg|_{\substack{x=x_0\\u=u_0}}$$

• Why do we require that $f(x_0, u_0) = 0$ in equilibrium?

- Why do we require that $f(x_0, u_0) = 0$ in equilibrium?
- This requires some thought. Indeed, we may talk about a *linear approximation* of any smooth function f at any point x₀:

 $f(x) \approx f(x_0) + f'(x_0)(x - x_0) \qquad -f(x_0)$ does not have to be 0

- Why do we require that $f(x_0, u_0) = 0$ in equilibrium?
- ► This requires some thought. Indeed, we may talk about a *linear approximation* of any smooth function f at any point x₀:

$$f(x) \approx f(x_0) + f'(x_0)(x - x_0) \qquad -f(x_0)$$
 does not have to be 0

The key is that we want to approximate a given nonlinear system x
 i = f(x, u) by a linear system x
 i = Ax + Bu (may have to shift coordinates: x → x - x₀, u → u - u₀)

- Why do we require that $f(x_0, u_0) = 0$ in equilibrium?
- ► This requires some thought. Indeed, we may talk about a *linear approximation* of any smooth function f at any point x₀:

$$f(x) \approx f(x_0) + f'(x_0)(x - x_0) \qquad -f(x_0)$$
 does not have to be 0

 The key is that we want to approximate a given nonlinear system x
 x = f(x, u) by a *linear* system x
 x = Ax + Bu (may have to shift coordinates: x → x - x₀, u → u - u₀)

Any linear system *must* have an equilibrium point at (x, u) = (0, 0):

$$f(x, u) = Ax + Bu$$
 $f(0, 0) = A0 + B0 = 0.$