## Plan of the Lecture

- Review: control, feedback, etc.
- Today's topic: state-space models of systems; linearization


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Goal: a general framework that encompasses all examples of interest. Once we have mastered this framework, we can proceed to analysis and then to design.

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- Review: control, feedback, etc.
- Today's topic: state-space models of systems; linearization

Goal: a general framework that encompasses all examples of interest. Once we have mastered this framework, we can proceed to analysis and then to design.

Reading: FPE, Sections 1.1, 1.2, 2.1-2.4, 7.2, 9.2.1. Chapter 2 has lots of cool examples of system models!!

## Notation Reminder

We will be looking at dynamic systems whose evolution in time is described by differential equations with external inputs.

We will not write the time variable $t$ explicitly, so we use

$$
\begin{array}{lll}
x & \text { instead of } & x(t) \\
\dot{x} & \text { instead of } & x^{\prime}(t) \text { or } \frac{\mathrm{d} x}{\mathrm{~d} t} \\
\ddot{x} & \text { instead of } & x^{\prime \prime}(t) \text { or } \frac{\mathrm{d}^{2} x}{\mathrm{~d} t^{2}}
\end{array}
$$

etc.

Example 1: Mass-Spring System


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Newton's second law (translational motion):

$$
\underbrace{F}_{\text {total force }}=m a
$$

## Example 1: Mass-Spring System



Newton's second law (translational motion):

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\underbrace{F}_{\text {total force }}=m a=\text { spring force }+ \text { friction }+ \text { external force }
$$

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Newton's second law (translational motion):
$\underbrace{F}_{\text {total force }}=m a=$ spring force + friction + external force
spring force $=-k x \quad$ (Hooke's law)
friction force $=-\rho \dot{x} \quad$ (Stokes' law — linear drag, only an approximation!!)

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F=-k x-\rho \dot{x}+u
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m \ddot{x}=-k x-\rho \dot{x}+u
$$

Move $x, \dot{x}, \ddot{x}$ to the LHS, $u$ to the RHS:

$$
m \ddot{x}+\rho \dot{x}+k x=u
$$

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Move $x, \dot{x}, \ddot{x}$ to the LHS, $u$ to the RHS:

$$
\ddot{x}+\frac{\rho}{m} \dot{x}+\frac{k}{m} x=\frac{u}{m}
$$

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\ddot{x}+\frac{\rho}{m} \dot{x}+\frac{k}{m} x=\frac{u}{m} \quad \text { 2nd-order linear ODE }
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Canonical form: convert to a system of 1st-order ODEs

## Example 1: Mass-Spring System



$$
\ddot{x}+\frac{\rho}{m} \dot{x}+\frac{k}{m} x=\frac{u}{m} \quad \text { 2nd-order linear ODE }
$$

Canonical form: convert to a system of 1st-order ODEs

$$
\begin{aligned}
\dot{x} & =v \quad \text { (definition of velocity) } \\
\dot{v} & =-\frac{\rho}{m} v-\frac{k}{m} x+\frac{1}{m} u
\end{aligned}
$$

## Example 1: Mass-Spring System



State-space model: express in matrix form

$$
\binom{\dot{x}}{\dot{v}}=\left(\begin{array}{cc}
0 & 1 \\
-\frac{k}{m} & -\frac{\rho}{m}
\end{array}\right)\binom{x}{v}+\binom{0}{\frac{1}{m}} u
$$

## Example 1: Mass-Spring System



State-space model: express in matrix form

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$$

Important: start reviewing your linear algebra now!!

- matrix-vector multiplication; eigenvalues and eigenvectors; etc.


## General n-Dimensional State-Space Model

$$
\text { state } x=\left(\begin{array}{c}
x_{1} \\
\vdots \\
x_{n}
\end{array}\right) \in \mathbb{R}^{n} \quad \text { input } u=\left(\begin{array}{c}
u_{1} \\
\vdots \\
u_{m}
\end{array}\right) \in \mathbb{R}^{m}
$$

## General n-Dimensional State-Space Model

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\begin{aligned}
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x_{1} \\
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x_{n}
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u_{1} \\
\vdots \\
u_{m}
\end{array}\right) \in \mathbb{R}^{m} \\
& \text { (0) (1) (0) (0) (C) }
\end{aligned}
$$

## General n-Dimensional State-Space Model

$$
\begin{gathered}
\text { state } x=\left(\begin{array}{c}
x_{1} \\
\vdots \\
x_{n}
\end{array}\right) \in \mathbb{R}^{n} \quad \text { input } u=\left(\begin{array}{c}
u_{1} \\
\vdots \\
u_{m}
\end{array}\right) \in \mathbb{R}^{m} \\
\left(\begin{array}{c}
\dot{x}_{1} \\
\vdots \\
\dot{x}_{n}
\end{array}\right)=\left(\begin{array}{c}
A \\
\\
n \times n \\
\text { matrix }
\end{array}\right)\left(\begin{array}{c}
x_{1} \\
\vdots \\
x_{n}
\end{array}\right)+\left(\begin{array}{c}
B \\
n \times m \\
\text { matrix }
\end{array}\right)\left(\begin{array}{c}
u_{1} \\
\vdots \\
u_{m}
\end{array}\right) \\
\dot{x}=A x+B u
\end{gathered}
$$

## Partial Measurements

$$
\text { state } x=\left(\begin{array}{c}
x_{1} \\
\vdots \\
x_{n}
\end{array}\right) \in \mathbb{R}^{n} \quad \text { input } u=\left(\begin{array}{c}
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\vdots \\
u_{m}
\end{array}\right) \in \mathbb{R}^{m} \\
\text { output } y & =\left(\begin{array}{c}
y_{1} \\
\vdots \\
y_{p}
\end{array}\right) \in \mathbb{R}^{p} \quad y=C x \quad C-p \times n \text { matrix }
\end{aligned}
$$

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\qquad \begin{array}{c}
\dot{x}=A x+B u \\
y=C x
\end{array}
\end{gathered}
$$

Example: if we only care about (or can only measure) $x_{1}$, then

$$
y=x_{1}=\left(\begin{array}{llll}
1 & 0 & \ldots & 0
\end{array}\right)\left(\begin{array}{c}
x_{1} \\
x_{2} \\
\vdots \\
x_{n}
\end{array}\right)
$$

State-Space Models: Bottom Line

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\begin{aligned}
& \dot{x}=A x+B u \\
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State-space models are useful and convenient for writing down system models for different types of systems, in a unified manner.

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When working with state-space models, what are states and what are inputs?

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State-space models are useful and convenient for writing down system models for different types of systems, in a unified manner.

When working with state-space models, what are states and what are inputs?

- match against $\dot{x}=A x+B u$


## Example 2: RL Circuit



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$$
-V_{S}+V_{R}+V_{L}=0, V_{S}
$$

Kirchhoff's voltage law Ohm's law

Faraday's law

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\begin{aligned}
-V_{S}+V_{R}+V_{L} & =0 \\
V_{R} & =R I \\
V_{L} & =L \dot{I}
\end{aligned}
$$

Kirchhoff's voltage law Ohm's law

Faraday's law

$$
\begin{gathered}
-V_{S}+R I+L \dot{I}=0 \\
\dot{I}=-\frac{R}{L} I+\frac{1}{L} V_{S} \quad(\text { 1st-order system })
\end{gathered}
$$

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(1st-order system)
$I$ - state, $V_{S}$ - input

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Q: How should we change the circuit in order to implement a 2nd-order system?

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(1st-order system)
$I$ - state, $V_{S}$ - input
Q: How should we change the circuit in order to implement a 2nd-order system? A: Add a capacitor.

## Example 3: Pendulum



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Newton's 2nd law (rotational motion):

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## Example 3: Pendulum



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$\underbrace{T}_{\substack{\text { toral } \\ \text { toraue }}}=\underbrace{J}_{\substack{\text { moment } \\ \text { of mextian acceleratation }}} \underbrace{\alpha}$ $=$ pendulum torque + external torque

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$=$ pendulum torque + external torque

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\text { pendulum torque }=\underbrace{-m g \sin \theta}_{\text {force }} \cdot \underbrace{\ell}_{\text {lever arm }}
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moment of inertia $J=m \ell^{2}$

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-m \mathrm{~g} \ell \sin \theta+T_{\mathrm{e}}=m \ell^{2} \ddot{\theta}
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$$
\ddot{\theta}=-\frac{\mathrm{g}}{\ell} \sin \theta+\frac{1}{m \ell^{2}} T_{\mathrm{e}} \quad \text { (nonlinear equation) }
$$

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For small $\theta$, use the approximation $\sin \theta \approx \theta$


$$
\ddot{\theta}=-\frac{\mathrm{g}}{\ell} \theta+\frac{1}{m \ell^{2}} T_{\mathrm{e}}
$$

State-space form: $\theta_{1}=\theta, \theta_{2}=\dot{\theta}$

$$
\dot{\theta}_{2}=-\frac{\mathrm{g}}{\ell} \theta+\frac{1}{m \ell^{2}} T_{\mathrm{e}}=-\frac{\mathrm{g}}{\ell} \theta_{1}+\frac{1}{m \ell^{2}} T_{\mathrm{e}}
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\begin{gathered}
\ddot{\theta}=-\frac{\mathrm{g}}{\ell} \theta+\frac{1}{m \ell^{2}} T_{\mathrm{e}} \\
\text { State-space form: } \theta_{1}=\theta, \theta_{2}=\dot{\theta} \\
\dot{\theta}_{2}=-\frac{\mathrm{g}}{\ell} \theta+\frac{1}{m \ell^{2}} T_{\mathrm{e}}=-\frac{\mathrm{g}}{\ell} \theta_{1}+\frac{1}{m \ell^{2}} T_{\mathrm{e}} \\
\binom{\dot{\theta}_{1}}{\dot{\theta}_{2}}=\left(\begin{array}{cc}
0 & 1 \\
-\frac{\mathrm{g}}{\ell} & 0
\end{array}\right)\binom{\theta_{1}}{\theta_{2}}+\binom{0}{\frac{1}{m \ell^{2}}} T_{\mathrm{e}}
\end{gathered}
$$

## Linearization

Taylor series expansion:

$$
\begin{aligned}
f(x) & =f\left(x_{0}\right)+f^{\prime}\left(x_{0}\right)\left(x-x_{0}\right)+\frac{1}{2} f^{\prime \prime}\left(x_{0}\right)\left(x-x_{0}\right)^{2}+\ldots \\
& \approx f\left(x_{0}\right)+f^{\prime}\left(x_{0}\right)\left(x-x_{0}\right) \quad \text { linear approximation around } x=x_{0}
\end{aligned}
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$$

Control systems are generally nonlinear:
$\dot{x}=f(x, u)$
nonlinear state-space model
$x=\left(\begin{array}{c}x_{1} \\ \vdots \\ x_{n}\end{array}\right) \quad u=\left(\begin{array}{c}u_{1} \\ \vdots \\ u_{m}\end{array}\right) \quad f=\left(\begin{array}{c}f_{1} \\ \vdots \\ f_{n}\end{array}\right)$

## Linearization

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$x=\left(\begin{array}{c}x_{1} \\ \vdots \\ x_{n}\end{array}\right) \quad u=\left(\begin{array}{c}u_{1} \\ \vdots \\ u_{m}\end{array}\right) \quad f=\left(\begin{array}{c}f_{1} \\ \vdots \\ f_{n}\end{array}\right)$
Assume $x=0, u=0$ is an equilibrium point: $f(0,0)=0$
This means that, when the system is at rest and no control is applied, the system does not move.

## Linearization

Linear approx. around $(x, u)=(0,0)$ to all components of $f$ :

$$
\dot{x}_{1}=f_{1}(x, u), \quad \ldots, \quad \dot{x}_{n}=f_{n}(x, u)
$$

## Linearization

Linear approx. around $(x, u)=(0,0)$ to all components of $f$ :

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\dot{x}_{1}=f_{1}(x, u), \quad \ldots, \quad \dot{x}_{n}=f_{n}(x, u)
$$

For each $i=1, \ldots, n$,

$$
\begin{aligned}
f_{i}(x, u)=\underbrace{f_{i}(0,0)}_{=0} & +\frac{\partial f_{i}}{\partial x_{1}}(0,0) x_{1}+\ldots+\frac{\partial f_{i}}{\partial x_{n}}(0,0) x_{n} \\
& +\frac{\partial f_{i}}{\partial u_{1}}(0,0) u_{1}+\ldots+\frac{\partial f_{i}}{\partial u_{m}}(0,0) u_{m}
\end{aligned}
$$

## Linearization

Linear approx. around $(x, u)=(0,0)$ to all components of $f$ :

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& +\frac{\partial f_{i}}{\partial u_{1}}(0,0) u_{1}+\ldots+\frac{\partial f_{i}}{\partial u_{m}}(0,0) u_{m}
\end{aligned}
$$

Linearized state-space model:

$$
\dot{x}=A x+B u, \quad \text { where } A_{i j}=\left.\frac{\partial f_{i}}{\partial x_{j}}\right|_{\substack{x=0 \\ u=0}}, B_{i k}=\left.\frac{\partial f_{i}}{\partial u_{k}}\right|_{\substack{x=0 \\ u=0}}
$$

## Linearization

Linear approx. around $(x, u)=(0,0)$ to all components of $f$ :

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\dot{x}_{1}=f_{1}(x, u), \quad \ldots, \quad \dot{x}_{n}=f_{n}(x, u)
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For each $i=1, \ldots, n$,

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$$

Important: since we have ignored the higher-order terms, this linear system is only an approximation that holds only for small deviations from equilibrium.

## Example 3: Pendulum, Revisited

Original nonlinear state-space model:

$$
\begin{aligned}
& \dot{\theta}_{1}=f_{1}\left(\theta_{1}, \theta_{2}, T_{\mathrm{e}}\right)=\theta_{2} \quad \text { already linear } \\
& \dot{\theta}_{2}=f_{2}\left(\theta_{1}, \theta_{2}, T_{\mathrm{e}}\right)=-\frac{\mathrm{g}}{\ell} \sin \theta_{1}+\frac{1}{m \ell^{2}} T_{\mathrm{e}}
\end{aligned}
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\end{aligned}
$$

Linear approx. of $f_{2}$ around equilibrium $\left(\theta_{1}, \theta_{2}, T_{\mathrm{e}}\right)=(0,0,0)$ :

$$
\begin{array}{lll}
\frac{\partial f_{2}}{\partial \theta_{1}}=-\frac{\mathrm{g}}{\ell} \cos \theta_{1} & \frac{\partial f_{2}}{\partial \theta_{2}}=0 & \frac{\partial f_{2}}{\partial T_{\mathrm{e}}}=\frac{1}{m \ell^{2}} \\
\left.\frac{\partial f_{2}}{\partial \theta_{1}}\right|_{0}=-\frac{\mathrm{g}}{\ell} & \left.\frac{\partial f_{2}}{\partial \theta_{2}}\right|_{0}=0 & \left.\frac{\partial f_{2}}{\partial T_{\mathrm{e}}}\right|_{0}=\frac{1}{m \ell^{2}}
\end{array}
$$

## Example 3: Pendulum, Revisited

Original nonlinear state-space model:

$$
\begin{aligned}
& \dot{\theta}_{1}=f_{1}\left(\theta_{1}, \theta_{2}, T_{\mathrm{e}}\right)=\theta_{2} \quad \text { - already linear } \\
& \dot{\theta}_{2}=f_{2}\left(\theta_{1}, \theta_{2}, T_{\mathrm{e}}\right)=-\frac{\mathrm{g}}{\ell} \sin \theta_{1}+\frac{1}{m \ell^{2}} T_{\mathrm{e}}
\end{aligned}
$$

Linear approx. of $f_{2}$ around equilibrium $\left(\theta_{1}, \theta_{2}, T_{\mathrm{e}}\right)=(0,0,0)$ :

$$
\begin{array}{lll}
\frac{\partial f_{2}}{\partial \theta_{1}}=-\frac{\mathrm{g}}{\ell} \cos \theta_{1} & \frac{\partial f_{2}}{\partial \theta_{2}}=0 & \frac{\partial f_{2}}{\partial T_{\mathrm{e}}}=\frac{1}{m \ell^{2}} \\
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\end{array}
$$

Linearized state-space model of the pendulum:

$$
\dot{\theta}_{1}=\theta_{2}
$$

$$
\dot{\theta}_{2}=-\frac{\mathrm{g}}{\ell} \theta_{1}+\frac{1}{m \ell^{2}} T_{\mathrm{e}} \quad \text { valid for small deviations from equ. }
$$

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- Start from nonlinear state-space model

$$
\dot{x}=f(x, u)
$$

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$$
\begin{aligned}
& \underline{x}=x-x_{0} \quad \underline{u}=u-u_{0} \\
& \underline{f}(\underline{x}, \underline{u})=f\left(\underline{x}+x_{0}, \underline{u}+u_{0}\right)=f(x, u)
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Note that the transformation is invertible:

$$
x=\underline{x}+x_{0}, \quad u=\underline{u}+u_{0}
$$

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- Pass to shifted variables $\underline{x}=x-x_{0}, \underline{u}=u-u_{0}$

$$
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& =\underline{f}(\underline{x}, \underline{u})
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$$

- Now linearize:

$$
\underline{\dot{x}}=A \underline{x}+B \underline{u}, \quad \text { where } A_{i j}=\left.\frac{\partial f_{i}}{\partial x_{j}}\right|_{\substack{x=x_{0} \\ u=u_{0}}}, B_{i k}=\left.\frac{\partial f_{i}}{\partial u_{k}}\right|_{\substack{x=x_{0} \\ u=u_{0}}}
$$

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$f(x) \approx f\left(x_{0}\right)+f^{\prime}\left(x_{0}\right)\left(x-x_{0}\right) \quad-f\left(x_{0}\right)$ does not have to be 0


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Any linear system must have an equilibrium point at $(x, u)=(0,0)$ :

$$
f(x, u)=A x+B u \quad f(0,0)=A 0+B 0=0
$$

