

ECE 486: Control Systems

- ▶ Lecture 19B: lead/lag control, Part II

Goal: introduce the use of lag dynamic compensators

Reading: FPE, Chapter 5

Lead & Lag Compensators

Consider a general controller of the form

$$K \frac{s + z}{s + p} \quad \text{— } K, z, p > 0 \text{ are design parameters}$$

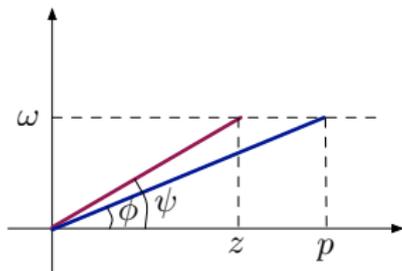
Depending on the relative values of z and p , we call it:

- ▶ a **lead compensator** when $z < p$
- ▶ a **lag compensator** when $z > p$

Why the name “lead/lag?” — think frequency response

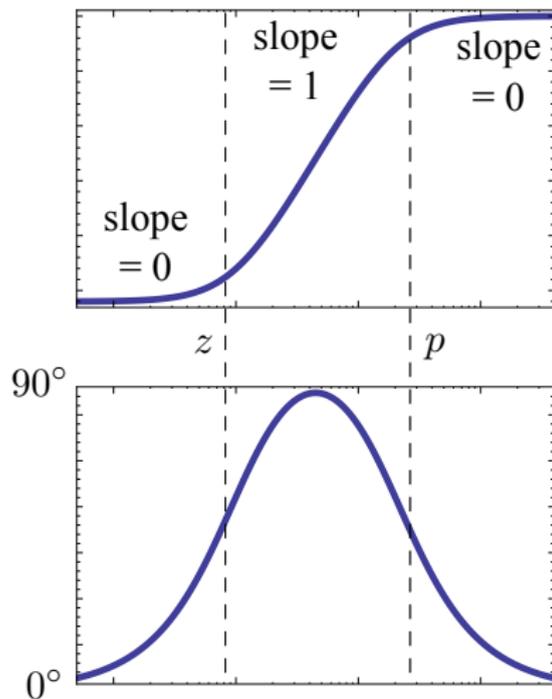
$$\angle \frac{j\omega + z}{j\omega + p} = \angle(j\omega + z) - \angle(j\omega + p) = \psi - \phi$$

- ▶ if $z < p$, then $\psi - \phi > 0$
(**phase lead**)
- ▶ if $z > p$, then $\psi - \phi < 0$
(**phase lag**)



Lead Compensation: Bode Plot

$$KD(s) = \frac{K \left(\frac{s}{z} + 1 \right)}{\left(\frac{s}{p} + 1 \right)}$$

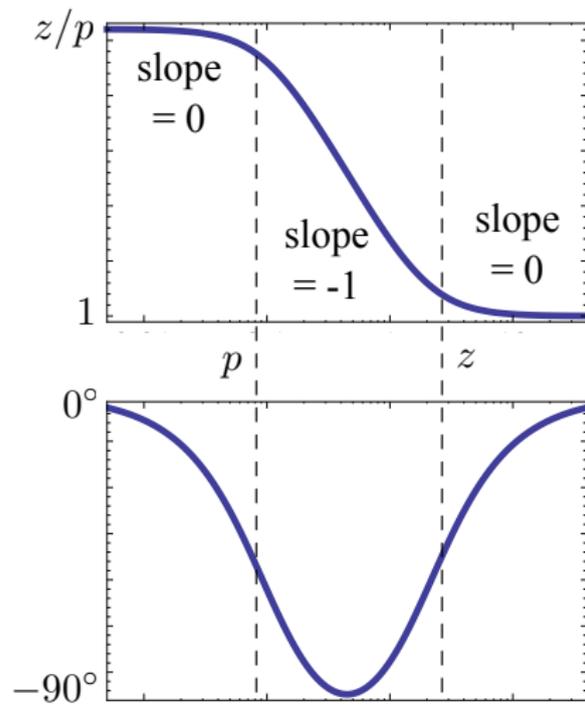


► magnitude levels off at high frequencies \implies better noise suppression

► adds phase, hence the term “phase lead”

Lag Compensation: Bode Plot

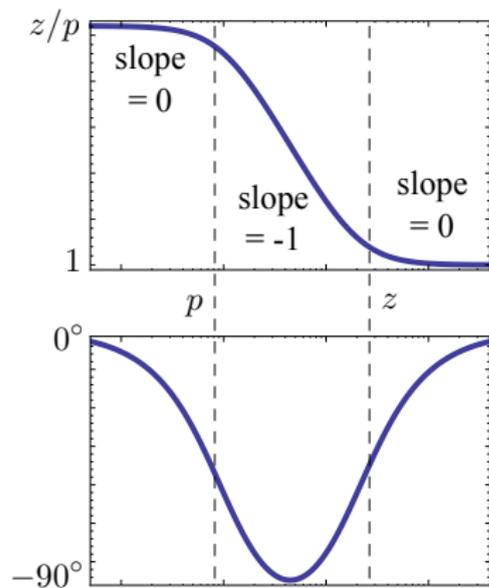
$$D(s) = \frac{s + z}{s + p} = \frac{z \frac{s}{z} + 1}{p \frac{s}{p} + 1}, \quad z \gg p$$



- ▶ $\frac{j\omega + z}{j\omega + p} \xrightarrow{\omega \rightarrow \infty} 1$
so $M \rightarrow 1$ at high frequencies

- ▶ subtracts phase, hence the term “phase lag”

Lag Compensation: Bode Plot



$$\blacktriangleright \frac{j\omega + z}{j\omega + p} \xrightarrow{\omega \rightarrow 0} \frac{z}{p}$$

steady-state tracking error:

$$e(\infty) = \left. \frac{sR(s)}{1 + D(s)G(s)} \right|_{s=0}$$

large $z/p \implies$ better s.s. tracking

- \blacktriangleright lag decreases $\omega_c \implies$ slows down time response (to compensate, adjust K or add lead)
- \blacktriangleright **caution:** lead increases PM, but adding lag can undo this
- \blacktriangleright to mitigate this, choose both z and p very small, while maintaining desired ratio z/p

Example

$$G(s) = \frac{1}{(s + 0.2)(s + 0.5)} \stackrel{\text{Bode form}}{=} \frac{10}{\left(\frac{s}{0.2} + 1\right) \left(\frac{s}{0.5} + 1\right)}$$

Objectives:

- ▶ $PM \geq 60^\circ$
- ▶ $e(\infty) \leq 10\%$ for constant reference (closed-loop tracking error)

Strategy:

- ▶ we will use lag

$$KD(s) = K \frac{s + z}{s + p}, \quad z \gg p$$

- ▶ z and p will be chosen to get good tracking
- ▶ PM will be shaped by choosing K
- ▶ this is different from what we did for lead (used p and z to shape PM, then chose K to get desired bandwidth spec)

Review: Lead Control Using Frequency Response

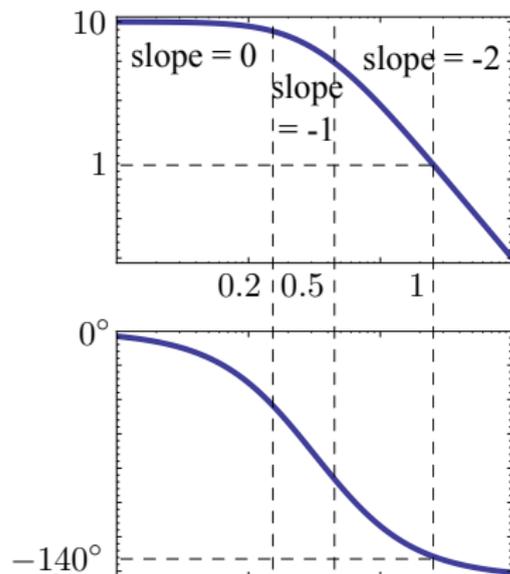
General Procedure

1. Choose K to get desired bandwidth spec w/o lead
2. Choose lead zero and pole to get desired PM
 - ▶ in general, we should first check PM with the K from 1, w/o lead, to see how much more PM we need
3. Check design and iterate until specs are met.

This is an intuitive procedure, but it's not very precise, requires trial & error.

Step 1: Choose K to Shape PM

Check Bode plot of $G(s)$ to see how much PM it already has:



► from Matlab, $\omega_c \approx 1$

► PM $\approx 40^\circ$

► we want PM = 60°

$$\phi = -120^\circ \quad \text{at } \omega \approx 0.573$$

$$M = 2.16$$

— need to decrease K to $1/2.16$

A conservative choice (to allow some slack) is $K = 1/2.5 = 0.4$, gives $\omega_c \approx 0.52$, PM $\approx 65^\circ$

Step 2: Choose z & p to Shape Tracking Error

So far: $KG(s) = \frac{0.4 \cdot 10}{\left(\frac{s}{0.2} + 1\right) \left(\frac{s}{0.5} + 1\right)}$

$$e(\infty) = \frac{1}{1 + KG(s)} \Big|_{s=0} = \frac{1}{1 + 4} = \frac{1}{5} = 20\% \quad (\text{too high})$$

To have $e(\infty) \leq 10\%$, need $KD(0)G(0) \geq 9$:

$$e(\infty) = \frac{1}{1 + KD(0)G(0)} \leq \frac{1}{1 + 9} = 10\%.$$

So, we need

$$D(0) = \frac{s + z}{s + p} \Big|_{s=0} = \frac{z}{p} \geq \frac{9}{4} = 2.25 \quad \text{— say, } z/p = 2.5$$

Not to distort PM and ω_c , let's pick z and p an order of magnitude smaller than $\omega_c \approx 0.5$: $z = 0.05$, $p = 0.02$

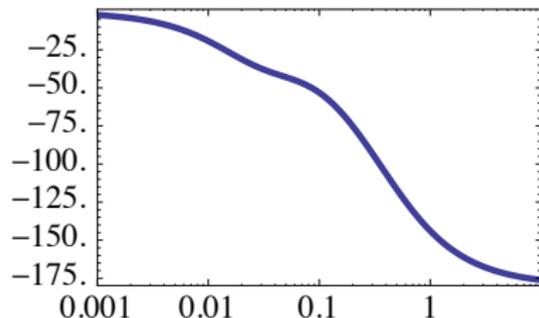
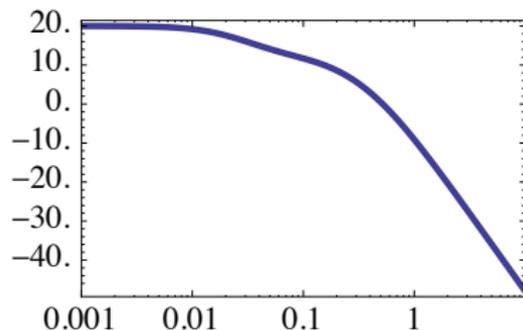
Overall Design

Plant:

$$G(s) = \frac{10}{\left(\frac{s}{0.2} + 1\right) \left(\frac{s}{0.5} + 1\right)}$$

Controller:

$$KD(s) = 0.4 \frac{s + 0.05}{s + 0.02}$$

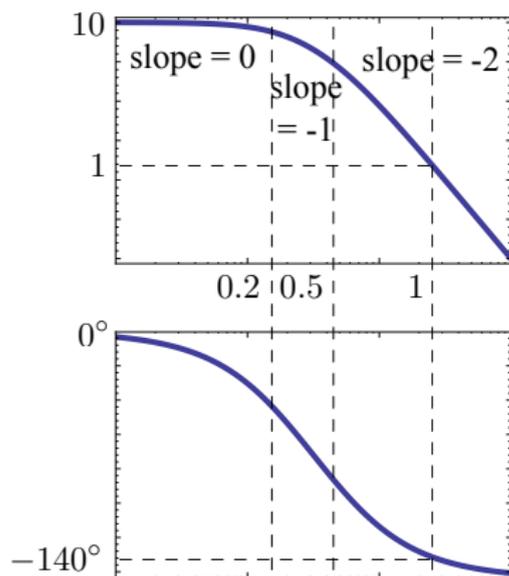


— the design still needs a bit of refinement ...

Lead & Lag Compensation

Let's combine the advantages of PD/lead and PI/lag.

Back to our example:
$$G(s) = \frac{10}{\left(\frac{s}{0.2} + 1\right) \left(\frac{s}{0.5} + 1\right)}$$



- ▶ from Matlab, $\omega_c \approx 1$
- ▶ PM $\approx 40^\circ$

New objectives:

- ▶ $\omega_{BW} \geq 2$
- ▶ PM $\geq 60^\circ$
- ▶ $e(\infty) \leq 1\%$ for const. ref.

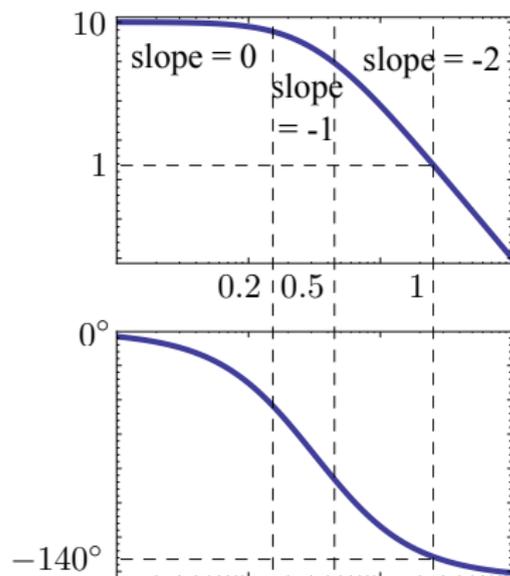
Lead & Lag Compensation

What we got before, with lag only:

- ▶ Improved PM by adjusting K to decrease ω_c .
- ▶ This gave $\omega_c \approx 0.5$, whereas now we want a larger ω_c (recall: $\omega_{\text{BW}} \in [\omega_c, 2\omega_c]$, so $\omega_c = 0.5$ is too small)

So: we need to reshape the phase curve using lead.

Lead & Lag Compensation



Step 1. Choose K to get $\omega_c \approx 2$
(before lead)

Using Matlab, can check:

at $\omega = 2$, $M \approx 0.24$ (with $K = 1$)

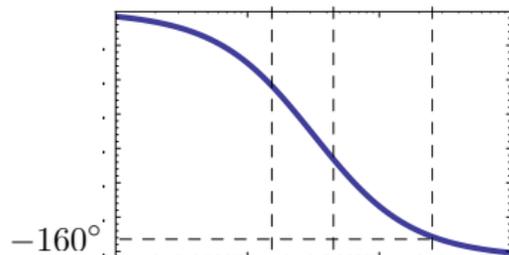
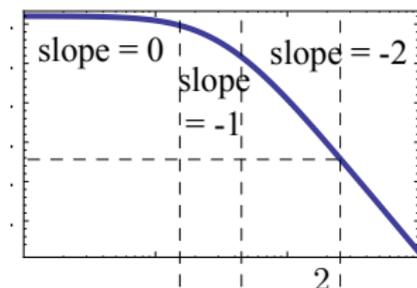
— need $K = \frac{1}{0.24} \approx 4.1667$

— choose $K = 4$

(gives ω_c slightly < 2 , but still ok).

Lead & Lag Compensation

$$K = 4$$



Step 2. Decide how much phase lead is needed, and choose z_{lead} and p_{lead}

Using Matlab, can check:

$$\text{at } \omega = 2, \quad \phi \approx -160^\circ$$

— so PM = 20°

(in fact, choosing $K = 4$ made things worse: it increased ω_c and consequently decreased PM)

We need at least 40° phase lead!!

The choice of lead pole/zero must satisfy

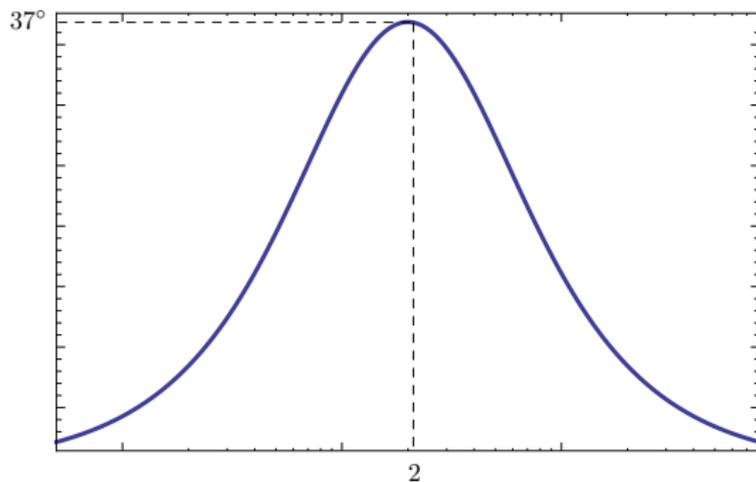
$$\sqrt{z_{\text{lead}} \cdot p_{\text{lead}}} \approx 2 \implies z_{\text{lead}} \cdot p_{\text{lead}} = 4$$

Lead & Lag Compensation

Need at least 40° phase lead, while satisfying

$$\sqrt{z_{\text{lead}} \cdot p_{\text{lead}}} \approx 2 \implies z_{\text{lead}} \cdot p_{\text{lead}} = 4$$

Let's try $z_{\text{lead}} = 1$ and $p_{\text{lead}} = 4$ $D(s) = \frac{s+1}{\frac{s}{4}+1}$



Phase lead = 37° — not enough!!

Lead & Lag Compensation

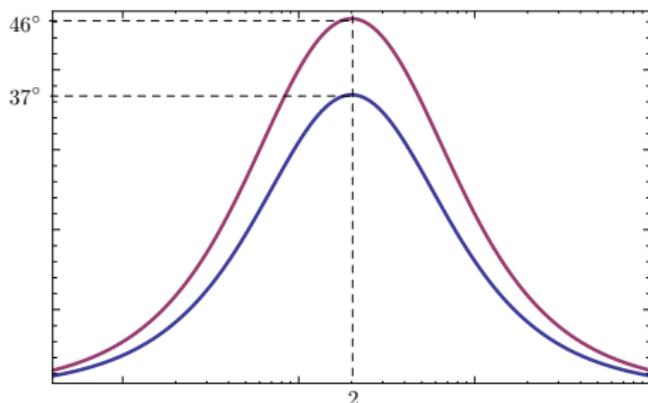
Need at least 40° phase lead, while satisfying

$$\sqrt{z_{\text{lead}} \cdot p_{\text{lead}}} \approx 2 \implies z_{\text{lead}} \cdot p_{\text{lead}} = 4$$

The choice of $z_{\text{lead}} = 1$, $p_{\text{lead}} = 4$ gave phase lead = 37° .

Need to space z_{lead} and p_{lead} farther apart:

$$\begin{cases} z_{\text{lead}} = 0.8 \\ p_{\text{lead}} = 5 \end{cases} \implies \text{phase lead} = 46^\circ$$



Lead & Lag Compensation

Step 3. Evaluate steady-state tracking and choose $z_{\text{lag}}, p_{\text{lag}}$ to satisfy specs

So far:

$$K \underbrace{D(s)}_{\substack{\text{lead} \\ \text{only}}} G(s) = 4 \frac{\frac{s}{0.8} + 1}{\frac{s}{5} + 1} \cdot \frac{10}{\left(\frac{s}{0.2} + 1\right) \left(\frac{s}{0.5} + 1\right)}$$

$$KD(0)G(0) = 40 \quad \implies \quad e(\infty) = \frac{1}{1 + KD(0)G(0)} = \frac{1}{1 + 40}$$

— this is not small enough: need $1\% = \frac{1}{100} = \frac{1}{1 + 99}$

We want $D(0) \geq \frac{99}{40}$ with lag $\frac{z_{\text{lag}}}{p_{\text{lag}}} \approx 2.5$ will do

Lead & Lag Compensation

Need to choose lag pole/zero that are sufficiently small (not to distort the phase lead too much) and satisfy $\frac{z_{\text{lag}}}{p_{\text{lag}}} \approx 2.5$.

We can stick with our previous design:

$$z_{\text{lag}} = 0.05, \quad p_{\text{lag}} = 0.02$$

Overall controller:

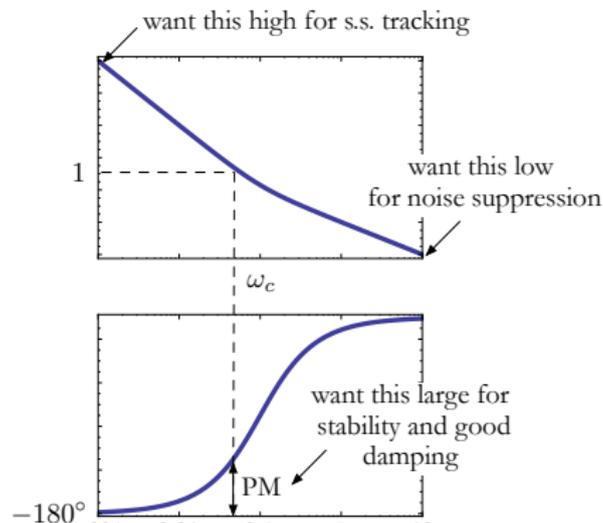
$$\underbrace{4 \frac{\frac{s}{0.8} + 1}{\frac{s}{5} + 1}}_{\text{lead (with gain } K = 4 \text{ absorbed)}} \cdot \underbrace{\frac{s + 0.05}{s + 0.02}}_{\text{lag (not in Bode form)}}$$

(Note: we don't rewrite lag in Bode form, because $z_{\text{lag}}/p_{\text{lag}}$ is not incorporated into K .)

Frequency Domain Design Method: Advantages

Design based on Bode plots is good for:

- ▶ easily visualizing the concepts



- ▶ evaluating the design and seeing which way to change it
- ▶ using experimental data (frequency response of the uncontrolled system can be measured experimentally)

Frequency Domain Design Method: Disadvantages

Design based on Bode plots is **not good for**:

- ▶ exact closed-loop pole placement (root locus is more suitable for that)
- ▶ deciding if a given K is stabilizing or not ...
 - ▶ we can only measure *how far* we are from instability (using GM or PM), if we know that we are stable
 - ▶ however, we don't have a way of checking whether a given K is stabilizing from frequency response data

The **Nyquist criterion** and Bode plots provide complementary benefits..