ECE 486: Control Systems

Lecture 8A: Proportional-Integral (PI) Control

Key Takeaways

This lecture describes proportional-integral control. The controller sets the plant input with two terms: (i) proportional to the error and (ii) proportional to the integral of the error.

Key properties of PI control:

- Integral control is that it achieves zero error in steady state (assuming system is stable and reaches a steady-state).
- 2. Initial transient is dominated by the proportional term while the steady state is dominated by the integral term.

The two terms in a PI controller can be used to provide better trade-offs in the control design.

Problem 1

Consider the following plant:

$$2\dot{y}(t) + 6y(t) = 8u(t)$$

with a PI controller in the following form:

$$u(t) = K_p e(t) + K_i \int_0^t e(\tau) d\tau$$

A) What is the ODE model for the closed-loop from *r* to *y*?

B) Choose (K_p, K_i) so that the closed-loop: i) is stable and ii) has $\zeta = 0.5$, iii) settling time $T_s \leq 0.5$ and (iv) zero steady-state error due to a unit step reference.

C) How will the response change if K_i is increased further? Would you recommend increasing K_i based on your analysis?

Solution 1A

$$2\dot{y}(t) + 6y(t) = 8u(t) u(t) = K_p e(t) + K_i \int_0^t e(\tau) d\tau$$

A) What is the ODE model for the closed-loop from r to y?

Solution 1B

$$2\dot{y}(t) + 6y(t) = 8u(t) u(t) = K_p e(t) + K_i \int_0^t e(\tau) d\tau$$

B) Choose (K_p, K_i) so that the closed-loop: i) is stable and ii) has $\zeta = 0.5$, iii) settling time $T_s \leq 3sec$, and (iv) zero steady-state error due to a unit step reference.

Solution 1C

$$2\dot{y}(t) + 6y(t) = 8u(t) u(t) = K_p e(t) + K_i \int_0^t e(\tau) d\tau$$

C) How will the response change if K_i is increased further? Would you recommend increasing K_i based on your analysis?

Solution 1-Extra Space

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Lecture 8B: Proportional-Derivative (PD) Control

Key Takeaways

This lecture describes proportional-derivative control. The controller sets the plant input with two terms: (i) proportional to the error and (ii) proportional to the derivative of the error.

Key properties of PD control:

- 1. Some plants cannot be stabilized by P or PI control. This motivates the use of PD.
- 2. A basic implementation of PD control will amplify noise.
- **3**. Common implementations use a "smoothed" derivative or a direct measurement the derivative of the output.

Problem 2

Consider the following plant:

$$\ddot{y}(t) - 2\dot{y}(t) + y(t) = u(t)$$

with a PD controller in the following form:

$$u(t) = K_p \left(r(t) - y(t) \right) - K_d \dot{y}(t)$$

A) What is the ODE model for the closed-loop from *r* to *y*?

B) Choose (K_p, K_d) so that the closed-loop: i) is stable and ii) has $(\omega_n, \zeta) = (2 \text{ rad/sec}, 0.5).$

C) What is the steady-state error if *r* is a unit step reference?

D) Would you increase or decrease Kp to reduce the steady-state error? What other impacts does this change have on the response?

Solution 2A

$$\ddot{y}(t) - 2\dot{y}(t) + y(t) = u(t)$$

$$u(t) = K_p \left(r(t) - y(t) \right) - K_d \dot{y}(t)$$

A) What is the ODE model for the closed-loop from r to y?

Solution 2B

$$\begin{split} \ddot{y}(t) - 2\dot{y}(t) + y(t) &= u(t) \\ u(t) &= K_p\left(r(t) - y(t)\right) - K_d \dot{y}(t) \\ \text{B) Choose } (\textit{K}_p,\textit{K}_d) \text{ so that the closed-loop: i) is stable and } \text{ ii) has } \\ (\omega_n,\zeta) &= (2 \text{ rad/sec, 0.5}). \end{split}$$

Solution 2C

$$\ddot{y}(t) - 2\dot{y}(t) + y(t) = u(t)$$
$$u(t) - K(r(t) - u(t)) - K\dot{u}(t)$$

$$u(\iota) - n_p(r(\iota) - g(\iota)) - n_d g(\iota)$$

C) What is the steady-state error if *r* is a unit step reference?

Solution 2D

$$\ddot{y}(t) - 2\dot{y}(t) + y(t) = u(t)$$

$$u(t) = K_p \left(r(t) - y(t) \right) - K_d \dot{y}(t)$$

D) Would you increase or decrease Kp to reduce the steady-state error? What other impacts does this change have on the response?

Solution 2-Extra Space