ECE 486: Control Systems

Lecture 7A: Summary Of Control Design Issues

Key Takeaways

Models used for control design are often simplified and contain a variety of inaccuracies.

 Uncertain parameters, unmodeled dynamics, nonlinear effects, and implementation effects.

Control design involves trade-offs to satisfy many conflicting objectives.

 Stability, reference tracking, disturbance rejection, actuator effort, noise rejection, and robustness to model uncertainty.

Problem 1

A control system is required to ensure the quadcopter below maintains a desired altitude.

- A) Discuss the simplified models that might be used for control design and various sources of inaccuracies.
- B) Discuss the various competing objectives that might arise in the design of this system.

DJI Phantom 4Pro (Photo: A. Savin, Re-use under Free Art License)



Solution 1A

A) Discuss the simplified models that might be used for control design and various sources of inaccuracies.

- · Aero dynamic Forces
 · Pituhing no han of good
 · All motors are perfectly identical
- . Motor dynamics and propeller aero are fast.
- . Saturation UECO, 500)
- . Parameter errors (m, Kg)

DJI Phantom 4Pro (Photo: A. Savin, Re-use under Free Art License)



Problem 1B

B) Discuss the various competing objectives that might arise in the design of this system.

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· Accorny of mintaining desired although
               · Overshout/Undershoot requirements (might cause a crush or unexpected pilot behavior)
            Risk /sett/hy Thies (Speed of Response)

Noise (Sensor)

Be Disporbance Frees
           (Reject)
Remain within motor
DJI Phantom 4Pro Robert To
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ECE 486: Control Systems

Lecture 7B: Open-Loop Control

Key Takeaways

This lecture describes open-loop control.

Open-loop control does not require a sensor and hence it can lead to a cheaper system. It can be effective if:

- 1. The plant is stable,
- 2. The disturbances are small, and
- 3. The model is accurate.

If any of these conditions fails, then open-loop control will either fail to achieve stability (if the plant is unstable) or will not provide accurate tracking.

Problem 2

Consider the following plant:

$$\ddot{y}(t) + 2\dot{y}(t) + 10y(t) = 20u(t) + 10d(t)$$

This system is underdamped with $\omega_n=3.16\frac{rad}{sec}$, $\zeta=0.316$, and poles $s_{1,2}=-1\pm 3j$.

- A) What is the model from inputs (r,d) to output y if we use an open-loop controller $u(t) = K_{ol} r(t)$?
- B) Can the gain K_{ol} be selected so that the control system is overdamped from r to y?
- C) Select K_{ol} so that $y(t) \to \bar{r}$ when $r(t) = \bar{r}$ and d(t) = 0.
- D) Sketch the response y with your gain Kol when r(t) = 2 and d(t) = 1. What is the impact of the disturbance?

Solution 2A

$$\ddot{y}(t) + 2\dot{y}(t) + 10\,y(t) = 20\,u(t) + 10\,d(t)$$

A) What is the model from inputs (r,d) to output y if we use an open-loop controller $u(t) = K_{ol} r(t)$?

Solution 2B

$$\ddot{y}(t) + 2\dot{y}(t) + 10\,y(t) = 20\,u(t) + 10\,d(t)$$

B) Can the gain K_{ol} be selected so that the control system is overdamped from r to y? U= Kol C

$$\ddot{y} + 2\dot{y} + 10\dot{y} = (20 \text{ KoI}) + 10 \text{ d}$$

$$G(5) = \frac{20 \text{ koI}}{5^2 + 25 + 10} - 1 \pm 3\dot{y}$$
Underdamped

Solution 2C

$$\ddot{y}(t) + 2\dot{y}(t) + 10\,y(t) = 20\,u(t) + 10\,d(t)$$

C) Select K_{ol} so that $y(t) \to \bar{r}$ when $r(t) = \bar{r}$ and d(t) = 0.

Solution 2D

$$\ddot{y}(t) + 2\dot{y}(t) + 10\,y(t) = 20\,u(t) + 10\,d(t)$$

D) Sketch the response y with your gain Kol when r(t) = 2 and d(t) = 1. What is the impact of the disturbance?

$$\frac{\ddot{y} + 7 \dot{y}}{7} + 7 \dot{y} = 10 \text{ T} + 16 \text{ d} = 30 - \frac{30}{2}$$

$$\int_{0.316}^{2} = 0.316$$

$$\int_{0.316}^{2} = \frac{11.35}{2} = \frac{30}{2} = \frac{11.35}{2} = \frac{30}{2} = \frac{30$$

ECE 486: Control Systems

Lecture 7C: Proportional (P) Control

Key Takeaways

This lecture describes closed-loop proportional control. The controller sets the plant input proportional to the error.

Closed-loop control can achieve higher performance but requires a sensor. $u = \mathcal{K}_{p}(r - y)$

Larger proportional gains:

- (i) improve reference tracking and disturbance rejection
- (ii) increase the closed-loop speed of response.

but:

- (i) require larger control inputs
- (ii) can excite unmodeled dynamics

Problem 3

Consider the following plant:

- A) What is the model from inputs (r,d) to output y if we use an proportional controller $u(t) = K_p (r(t) y(t))$?
- B) Select K_p so that the steady-state error $\bar{e}=\bar{r}-\bar{y}$ is less than 0.1 when $r(t)=\bar{r}=2$ and d(t)=1.
- C) Sketch the response y with your gain K_p when r(t) = 2 and d(t) = 1. What is the time constant of the closed-loop?

Solution 3A

$$2\dot{y}(t) + 3y(t) = -4u(t) + d(t)$$

A) What is the model from inputs (r,d) to output y if we use an proportional controller $u(t) = K_p(r(t) - y(t))$?

$$2\dot{y} + 3\dot{y} = -4 k_p (r-\dot{y}) + d$$

$$7\dot{y} + (3 - 4k_p)\dot{y} = -4k_p r + d$$

Solution 3B

$$2\dot{y}(t) + 3y(t) = 4u(t) + d(t)$$

B) Select K_p so that the steady-state error $\bar{e}=\bar{r}-\bar{y}$ is less than

0.1 when $r(t) = \bar{r} = 2$ and d(t) = 1.

Solution 3C

$$2\dot{y}(t) + 3y(t) = -4u(t) + d(t)$$

C) Sketch the response y with your gain K_p when r(t) = 2 and d(t) = 1. What is the time constant of the closed-loop?

$$K_{p}=-160$$
 $2\dot{y}+(3-4)\dot{p})y=-4k_{p}r+d$
 $-2\dot{y}+(403)y=400t+d$
 $\dot{y}+\frac{403}{2}\dot{y}+200r+\dot{q}$ $T=\frac{3}{403}$ Sec = 0.0050
 $T_{5}=3T=\frac{3}{2}$ 0.0150

