

# Plan of the Lecture

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- ▶ **Today's topic:** dynamic response (transient and steady-state) with arbitrary I.C.'s

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*Goal:* develop a methodology for characterizing the output of a given system for a given input.

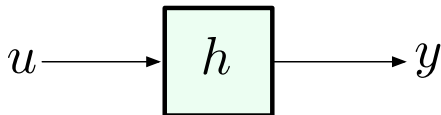
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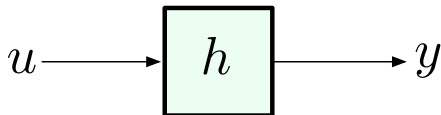
*Reading:* FPE, Section 3.1, Appendix A

## Dynamic Response



**Problem:** compute the response  $y$  to a given input  $u$  under a given set of initial conditions.

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In particular, we wish to know both the **transient response** (due to I.C.'s) and the **steady-state response** (once the effect of the I.C.'s “washes away”).

# Laplace Transforms Revisited

(see FPE, Appendix A)

One-sided (or unilateral) Laplace transform:

$$\mathcal{L}\{f(t)\} \equiv F(s) = \int_0^{\infty} f(t)e^{-st} dt \quad (\text{really, from } 0^-)$$

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— this is valid provided  $\text{Re}(s) > 0$ , so that  $e^{-st} \xrightarrow{t \rightarrow +\infty} 0$ .

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— in both cases, require  $\text{Re}(s) > 0$ , i.e.,  $s$  must lie in the right half-plane (RHP)

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for  $\text{Re}(s) > 0$

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— can't find  $Y(s)$  in the tables. So how do we compute  $y$ ?

## Method of Partial Fractions

Problem: compute  $\mathcal{L}^{-1} \left\{ \frac{s}{(s+1)(s^2+1)} \right\}$

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$$\frac{1}{s^2+1} \quad \mathcal{L}^{-1} \left\{ \frac{1}{s^2+1} \right\} = \sin t \quad (\#17)$$

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This brings us to the [method of partial fractions](#):

- ▶ boring (i.e., character-building), but *very useful*
- ▶ allows us to break up complicated fractions into sums of simpler ones, for which we know  $\mathcal{L}^{-1}$  from tables

## Method of Partial Fractions

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► Find  $a$ : multiply by  $s+1$  to isolate  $a$

$$(s+1)Y(s) = \frac{s}{s^2+1} = a + \frac{(s+1)(as+b)}{(s^2+1)}$$

— now let  $s = -1$  to “kill” the second term on the RHS:

$$a = (s+1)Y(s) \Big|_{s=-1} = -\frac{1}{2}$$

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— the freq. response formula gives only the steady-state part!!

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Therefore, the first formula is correct.

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— we will now see how to deal with nonzero I.C.'s ...

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Similarly:

$$\begin{aligned}\mathcal{L}\{f''(t)\} &= \mathcal{L}\{(f'(t))'\} = s\mathcal{L}\{f'(t)\} - f'(0) \\ &= s^2F(s) - sf(0) - f'(0)\end{aligned}$$

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## Example (continued)

$$\ddot{y} + 3\dot{y} + 2y = u, \quad y(0) = \alpha, \dot{y}(0) = \beta$$

Compute the *step response*, i.e., response to  $u(t) = 1(t)$

*Caution!!*  $Y(s) = H(s)U(s)$  no longer holds if  $\alpha \neq 0$  or  $\beta \neq 0$

Again, take Laplace transforms of both sides, mind the I.C.'s:

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*Note:* if  $\alpha = \beta = 0$ , then  $Y(s) = \frac{1}{s(s+1)(s+2)} = H(s)U(s)$

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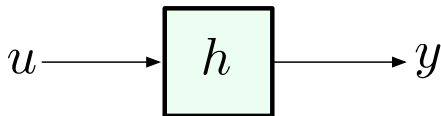
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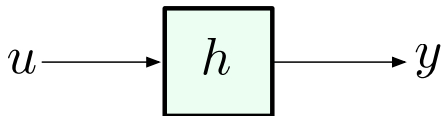
- ▶ the steady-state part is  $\frac{1}{2}\mathbf{1}(t)$  — converges to steady-state value of  $1/2$

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**Definition:** the steady-state value of the step response is called the *DC gain* of the system.

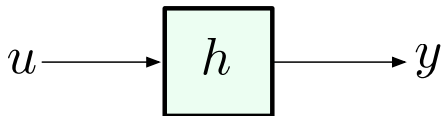
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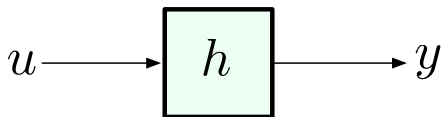
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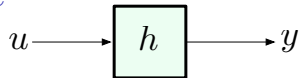
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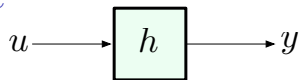
$$y(t) = \frac{1}{2}1(t) + (2\alpha + \beta - 1)e^{-t} + (1/2 - \alpha - \beta)e^{-2t}$$

therefore, DC gain =  $y(\infty) = 1/2$

## Steady-State Value



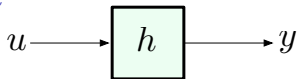
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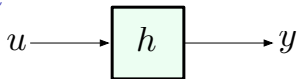
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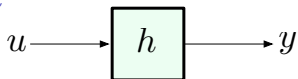


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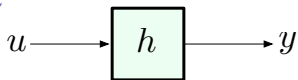
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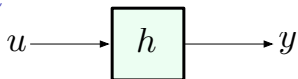
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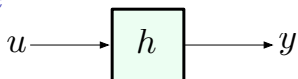
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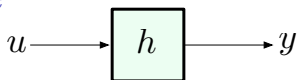
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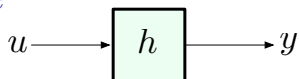
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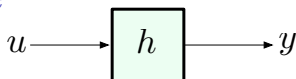
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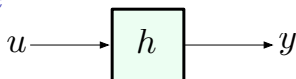
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## The Final Value Theorem

We can now deduce the **Final Value Theorem (FVT)**:

If all poles of  $sY(s)$  are *strictly stable* or lie in the *open left half-plane* (OLHP), i.e., have  $\text{Re}(s) < 0$ , then

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In our examples, multiply  $Y(s)$  by  $s$ , check poles:

- ▶  $Y(s) = \frac{1}{s+a}$        $sY(s) = \frac{s}{s+a}$   
if  $a > 0$ , then  $y(\infty) = 0$ ; if  $a < 0$ , FVT does not give correct answer
- ▶  $Y(s) = \frac{1}{s^2 + \omega^2}$        $sY(s) = \frac{s}{s^2 + \omega^2}$   
poles are purely imaginary (not in OLHP), FVT does not give correct answer
- ▶  $Y(s) = \frac{c}{s}$        $sY(s) = c$

## The Final Value Theorem

We can now deduce the **Final Value Theorem (FVT)**:

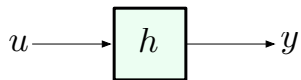
If all poles of  $sY(s)$  are *strictly stable* or lie in the *open left half-plane* (OLHP), i.e., have  $\text{Re}(s) < 0$ , then

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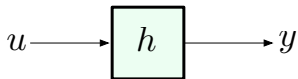
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poles are purely imaginary (not in OLHP), FVT does not give correct answer
- ▶  $Y(s) = \frac{c}{s}$        $sY(s) = c$   
poles at infinity, so  $y(\infty) = c$  – FVT gives correct answer

## Back to DC Gain

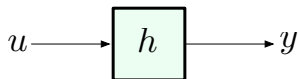


## Back to DC Gain



Step response:  $Y(s) = \frac{H(s)}{s}$

## Back to DC Gain



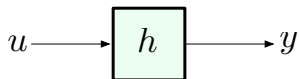
Step response:  $Y(s) = \frac{H(s)}{s}$

— if all poles of  $sY(s) = H(s)$  are strictly stable, then

$$y(\infty) = \lim_{s \rightarrow 0} H(s)$$

by the FVT.

## Back to DC Gain



Step response:  $Y(s) = \frac{H(s)}{s}$

— if all poles of  $sY(s) = H(s)$  are strictly stable, then

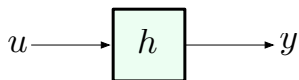
$$y(\infty) = \lim_{s \rightarrow 0} H(s)$$

by the FVT.

**Example:** compute DC gain of the system with transfer function

$$H(s) = \frac{s^2 + 5s + 3}{s^3 + 4s + 2s + 5}$$

## Back to DC Gain



Step response:  $Y(s) = \frac{H(s)}{s}$

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by the FVT.

**Example:** compute DC gain of the system with transfer function

$$H(s) = \frac{s^2 + 5s + 3}{s^3 + 4s + 2s + 5}$$

All poles of  $H(s)$  are strictly stable (we will see this later using the *Routh–Hurwitz criterion*), so

$$y(\infty) = H(s) \Big|_{s=0} = \frac{3}{5}.$$