

**Reading:** FPE, Sections 5.1, 5.2, 5.6.1.

**Problems:**

1. The goal of this exercise is to compare sensitivity of open-loop and closed-loop control with respect to errors in the *control gain*. Consider the DC motor model discussed in class, with no disturbance ( $w_\ell = 0$ ). Let the control gain sensitivity be defined as follows: when the controller gain changes from  $K$  to  $K + \delta K$  and, as a result, the steady state gain (DC gain) of the overall system changes from  $T$  to  $T + \delta T$ , we define  $S_K = \frac{\delta T/T}{\delta K/K}$ . (The motor gain  $A$  remains fixed here.)

a) Compute the sensitivity  $S_K$  in the open-loop case, starting from the nominal values  $K_{ol} = 1/A$  and  $T_{ol} = 1$ .

b) Compute the sensitivity  $S_K$  for a feedback gain  $K_{cl}$ , using the approximate formula  $\delta T = \frac{dT}{dK}\delta K$  and the fact that the nominal system gain is, as derived in class,  $T_{cl} = \frac{AK_{cl}}{1 + AK_{cl}}$ .

Hint: your final answers in a) and b) should be the same as the ones derived in class for sensitivity to errors in the motor gain  $A$ .

2. Suppose that the DC motor discussed in class is connected in feedback with a PI controller  $k_P + k_I/s$ . (This refers to the standard feedback control configuration, where the input to the controller is  $e = r - y = \omega_{ref} - \omega_m$ .) Write down the full transfer function of the closed-loop system in the presence of load/disturbance  $w_\ell$ . (For  $k_I = 0$  this should match what we derived in class for constant feedback gain.) Is it true that by proper choice of gains  $k_P$  and  $k_I$  we can achieve arbitrary pole placement as well as perfect constant reference tracking and constant disturbance rejection in steady state? Justify your answer.

3. Consider the plant with transfer function  $L(s) = \frac{1}{s^2 + 2s}$ . Under the action of a constant feedback gain  $K$ , the closed-loop poles are the roots of the characteristic polynomial  $s^2 + 2s + K$ .

a) Draw the (positive) root locus. (Use the expression for the closed-loop poles in terms of  $K$  obtained via the quadratic formula.)

b) Consider the settling time spec  $t_s \leq 4$ . Give some value (or range of values) of  $K$  for which the closed-loop system meets this spec. Justify your choice. Show the corresponding pole locations on the root locus.

c) Consider the rise time spec  $t_r \leq 1$ . Give some value (or range of values) of  $K$  for which the closed-loop system meets this spec. Justify your choice. Show the corresponding pole locations on the root locus.

d) Consider the overshoot spec  $M_p \leq 0.1$ . Give some value (or range of values) of  $K$  for which the closed-loop system meets this spec. Justify your choice. Show the corresponding pole locations on the root locus.

e) Suppose that it is desired to place the closed-loop poles at  $-1 \pm j$ . Find the value of  $K$  that will achieve this, using the characteristic equation  $s^2 + 2s + K = 0$  *but without using the quadratic formula*. (In other words, you should find a way of doing this that would also work for a higher-order example.)

4. Consider the following transfer functions:

$$1) L(s) = \frac{1}{s(s^2 + 4s + 8)} \qquad 2) L(s) = \frac{s}{(s - 1)(s + 1)^3}$$

For each one of these, do the following:

- a) Mark the zeros and poles on the  $s$ -plane and plot the real-axis part of the root locus.
- b) Use the phase condition from class to test whether or not the point  $s = j$  is on the root locus. If you run into “non-obvious” angles, *estimate* rather than *calculate* them, this should be enough.
- c) Determine asymptotes and departure and arrival angles. Plot the root locus branches based on this information.
- d) Determine imaginary-axis crossings (if any), and complete the (positive) root locus by using Rule 6 to check for multiple roots.
- e) Plot the (positive) root locus using the MATLAB `rlocus` command.

Turn in your MATLAB plots as well as hand sketches of root loci along with all accompanying calculations and explanations.