# **Inductive Charging Case**

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Design Review - ECE 445 Spring 2017

# Table of contents

| 1. |                                    |    |
|----|------------------------------------|----|
|    | 1.1 Objective                      | 3  |
|    | 1.2 Background                     |    |
|    | 1.3 High level requirements        | 3  |
| 2. | Design                             | 4  |
|    | 2.1 Block diagram                  |    |
|    | 2.2 Power module                   |    |
|    | 2.2.1 Description                  |    |
|    | 2.2.2 Circuit schematic            |    |
|    | 2.2.3 Calculations                 | E  |
|    | 2.2.4 Plots                        | E  |
|    | 2.3 DC-AC module                   | 8  |
|    | 2.3.1 Description                  | 8  |
|    | 2.3.2 Schematic                    |    |
|    | 2.3.3 Calculations                 | g  |
|    | 2.3.4 Plots                        | 10 |
|    | 2.4 Software module                | 11 |
|    | 2.4.1 Description                  | 11 |
|    | 2.4.2 Schematics                   | 11 |
|    | 2.5 Requirements and verifications | 12 |
|    | 2.6 Tolerance analysis             | 13 |
| 3. | Cost and Schedule                  | 15 |
|    | 3.1 Cost analysis                  | 15 |
|    | 3.1.1 Labor                        |    |
|    | 3.1.2 Parts                        | 15 |
|    | 3.1.3 Grand Total                  | 17 |
|    | 3.2 Schedule                       |    |
| 4. | Ethics and safety                  | 19 |
|    | 4.1 Safety statement               |    |
|    | 4.2 Ethics statement               |    |
|    |                                    |    |
| Re | eferences                          | 20 |

#### 1. Introduction

#### 1.1 Objective

As USB type C is becoming more common in phones, many companies are removing the headphone jack on phones [1]. This creates a big problem for those who want to transfer data or listen to music while charging their phone. This problem increases as phones become more powerful and their battery life do not grow at the same rate. It is very common to run out of battery at the end of the day after having used your phone during the whole day.

Our idea to solve this problem is to develop a rechargeable wireless battery that can give your phone an extra amount of power without taking up the only jack the phone has. We will implement a Qi transmitter circuit into a case along with the rechargeable battery. Power will flow from the battery to the transmitter circuit and will be received by the circuit integrated in our phone.

#### 1.2 Background

Nowadays there are some phone cases that allow you to charge your phone without plugging it into the socket [2]. Our device is different because we are going to use a system that transmits the power wirelessly. In the already existing cases, the rechargeable battery is directly connected to the charging port. These cases partially solve our problem as you do not need the phone to be connected to the wall, but we want to completely solve it by charging the phone wirelessly so we can use the port for other purposes.

#### 1.3 High level requirements

- The system has to be able to delivering 1000 mAh to the phone.
- The system has to deliver 5 W to the receiving coil.
- The system efficiency has to be greater than 70%.

# 2. Design

## 2.1 Block diagram

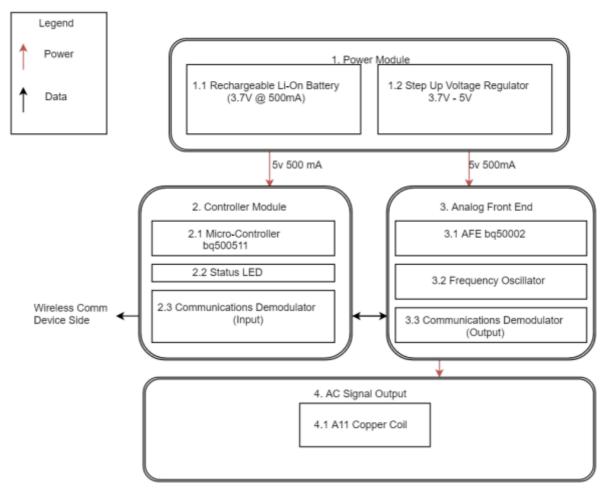


Figure 1: Block diagram

#### 2.2 Power module

#### 2.2.1 Description

#### 2.2.1.1 Battery

We are using a lithium ion polymer battery to power our circuit. These units are rechargeable and have undergone penetration as well as extreme heat testing. Capacity ranges from 200 mAh to 2000 mAh changing battery thickness from 1mm to 3.6mm. [3]

| Nominal Voltage           | 3.7V                |                   |
|---------------------------|---------------------|-------------------|
| Charging Cut-off Voltage  | 4.20V               |                   |
| Discharge Cut-off Voltage | 3.0V                |                   |
| Max. Charging Current     | 1C                  |                   |
| Max. Discharging Current  | 2C                  |                   |
| On and the Towns and the  | Charge 0~45℃        |                   |
| Operating Temperature     | Discharge –20~60°C  |                   |
| Storage Temperature       | -20~45℃ for 1Month  |                   |
| Storage Temperature       | -20~35℃ for 6Months |                   |
| Impedance                 | 180mΩ               | Maximum value     |
| Weight                    | 6g                  | Approximate value |

**Table 1: Battery specifications** 

#### 2.2.1.2 Step up voltage regulator

We are using the LM2621 as a high efficiency, step up DC-DC switch regulator for low voltage input systems. It can accept an input voltage between 1.2V and 14V, and can output a regulated voltage in the range [1.24V, 14V]. We want to output a voltage of 5V from an input of 2-3V.

#### 2.2.2 Circuit schematic

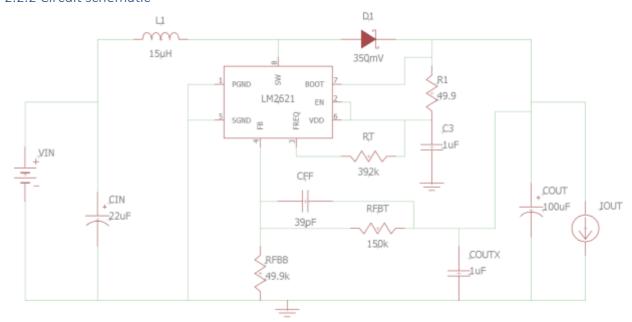


Figure 2: Power module schematic

#### 2.2.3 Calculations

$$RFBB = \frac{RFBT}{\frac{Vout}{Vmin} - 1} = \frac{150k}{\frac{5}{1.24} - 1} = 49.9k \approx 50k$$

$$Z(\omega) = j\omega Lm + \frac{\frac{j\omega Lp}{j\omega Cm}}{j\omega Lp + \frac{1}{j\omega Cm}} = \frac{j(\omega^3 Lm Lp Cm - \omega(Lm + Lp))}{\omega^2 Lp Cm - 1}$$

$$\omega_2^2 Lm Lp Cm - \omega_2(Lm + Lp) = 0$$

$$\omega_2 = \sqrt{\frac{Lm + Lp}{Lm Lp Cm}}$$

$$\omega_1^2 Lp Cm - 1 = 0$$

$$\omega_1 = \sqrt{\frac{1}{Lp Cm}}$$

As the frequency ranges from 110 kHz to 205 kHz, we choose Lp =  $6.3 \mu$ H and Cm =  $22 \mu$ F.

#### 2.2.4 Plots

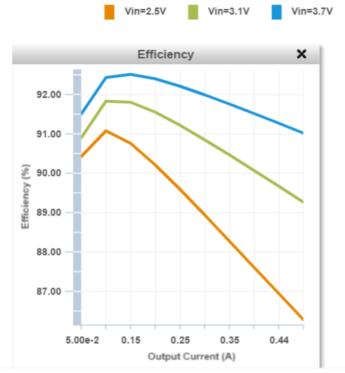


Figure 3: Power module. Efficiency vs. Output current

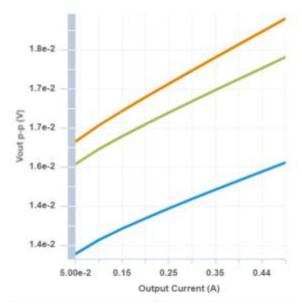


Figure 4: Power module. Output voltage ripple vs. Output current

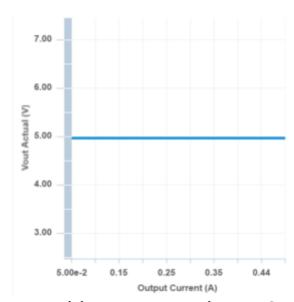


Figure 5: Power module. Mean output voltage vs. Output current

#### 2.3 DC-AC module

#### 2.3.1 Description

#### 2.3.1.1 Analog Front End bg50002

The bq50002 [4] device is a highly integrated wireless power transmitter analog front end (AFE) that contains all of the analog components required to implement a Wireless Power Consortium (WPC) compliant 5-V transmitter. The bq50002 device integrates a full-bridge power driver with MOSFETs, variable-frequency oscillator, two-channel communication demodulator, linear regulator, and protection circuits. The bq50002 device must be used together with the digital controller bq500511 to realize a compact two chip wireless power transmitter solution.

#### 2.3.1.2 Micro-controller bg500511

The bq500511 [5] is a wireless power transmitter controller that, when combined with the bq50002 analog front end device, integrates all functions required to create a Qi-compliant or proprietary 5-V transmitter. The bq500511 pings the surrounding environment for the receiver devices to be powered, safely engages the device, receives packet communication from the powered device and manages the power transfer according to WPC v1.2 specifications.

#### 2.3.1.3 Transmitting coil

We are using an A11 type copper coil. It is compliant with Qi and WPC standards.

#### 2.3.2 Schematic

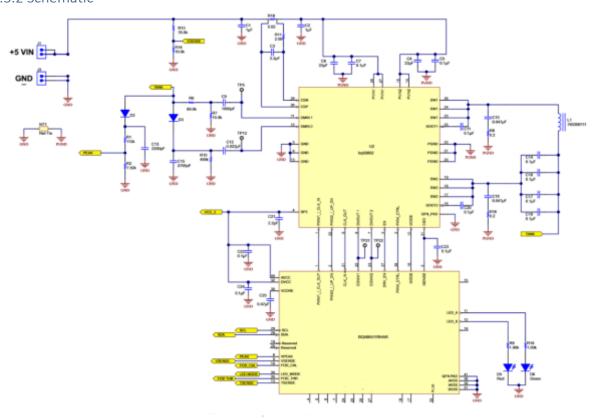


Figure 6: DC-AC module schematic

#### 2.3.3 Calculations

Corresponds to LED control option 8. Standby correlates to both LEDs being off. The red LED turns on when charging occurs. Once the phone is fully charged, the red LED will turn off and the green LED will turn on. Both LEDs will blink if a fault has occurred. [6]

 $R_{LED} = 200k \Omega$ 

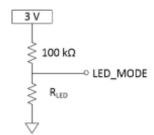


Figure 7: LED control

For the FOD (Foreign Object Detection) system, it is based off of input voltage.

FOD threshold = input voltage \* 400 = maximum allowed loss in mW.

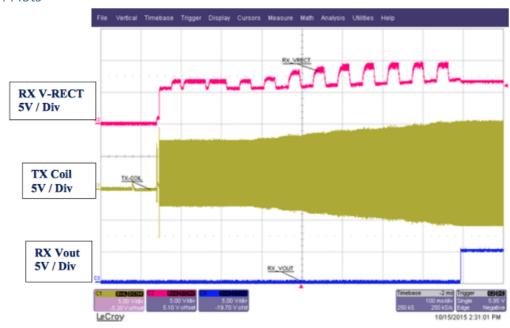


Figure 8: DC-AC module. Transition from standby

It shows a typical start up behavior for the TX and RX as the RX is placed on a TX in standby. The RX and TX can be seen transitioning from standby. (TX transmitter, RX receiver).

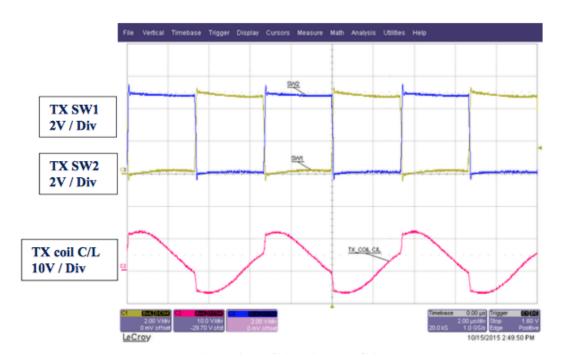


Figure 9: DC-AC module. Power transfer mode

It shows the transmitter operating in power transfer mode with a load of about 5-W. The coil drive signal is a 50% duty cycle signal 180 degrees out of phase. Operating frequency will change with load between 110 kHz and 205 kHz, at this point frequency is about 150 kHz.

#### 2.4 Software module

#### 2.4.1 Description

For our software module, we will develop a mobile app (Android), to enable user control, and present battery statistics, and other useful information. The application will communicate with the controller module, specifically with the bq500511 and bq50002a wireless power transmitter chips, that integrate all functions of a Qi-compliant wireless charger pad. These chips have communication ports that will transfer data to/from the cellular device. The app will read in data from the chips, and also send signals to the circuit to switch on/off the charging. We will continue to brainstorm features to add to the application to make the user experience better. To detect signals, I will use the *BatteryManager* class, which is in the Android SDK. [7] If it is not possible to communicate with the chips, then we plan to build a Wi-Fi module in the circuit to communicate with the application.

#### Technology stack:

- Android Studio as IDE (Integrated Development Environment)
- Java for controller and data logic
- XML for view
- Android emulator for basic testing
- Actual Android device for thorough testing.

#### 2.4.2 Schematics

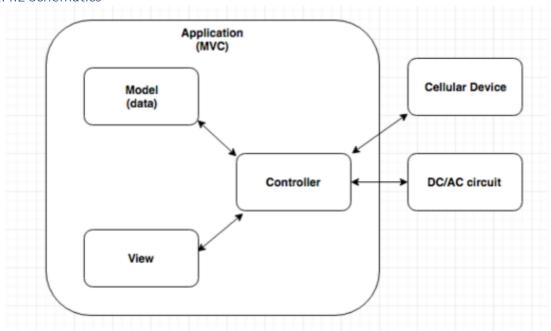


Figure 10: Software module schematic

# 2.5 Requirements and verifications

| Module | Requirements                | Verification procedures     |
|--------|-----------------------------|-----------------------------|
| Power  | The fluctuation of output   | This will be tested using   |
|        | voltage from the DC-DC      | only the power module.      |
|        | circuit must not be more    | We will hook up a           |
|        | than .1V (i.e. the voltage  | multimeter to the output    |
|        | should only range from      | of the step up circuit and  |
|        | 4.9V to 5.1V).              | take voltage values using a |
|        |                             | constant DC input as a      |
|        |                             | source and then the         |
|        |                             | lithium ion battery as a    |
|        |                             | source.                     |
|        | The voltage from the        | We will test this by again  |
|        | battery should always be    | using a multimeter to       |
|        | in the rated voltage range  | measure battery output      |
|        | for the IC (1.2V - 14V).    | voltage. This will be done  |
|        |                             | until the battery is        |
|        |                             | completely drained.         |
|        | The output current cannot   | We will perform the same    |
|        | exceed the IC's peak        | test as the voltage test,   |
|        | current of 2.85A.           | instead measuring           |
|        |                             | current. Again, we will use |
|        |                             | a constant DC source as     |
|        |                             | well as a battery source in |
|        |                             | order to gauge how          |
|        |                             | different inputs affect our |
|        |                             | output current.             |
| DC-AC  | The DC input voltage into   | We will test it with a      |
|        | AFE should not exceed 7V.   | multimeter.                 |
|        | The AC signal frequency     | We will check the           |
|        | has to be in range (110     | frequency of the AC signal  |
|        | kHz – 205 kHz) for the      | with the help of an         |
|        | right operation of the      | oscilloscope.               |
|        | charging receiving circuit. |                             |
|        | The LED system works.       | We will check the phone     |
|        |                             | battery charge when the     |
|        | 2. Doguiromonto and verific | green LED turns on.         |

Table 2: Requirements and verifications

#### 2.6 Tolerance analysis

For our tolerance analysis, we are examining the Wurth Electronics A11 TX coil [8]. It's crucial to understand the limiters of the coil as a fault in the coil will prove catastrophic to the entire circuit. As seen in figure 11, the inductance value of the coil does not change with the current, so we don't have to be too concerned with small variations in current affecting our transmitter. What we must be careful of is the frequency values as they have a major effect on the system (shown in figure 12). Our microcontroller will keep us under 205khz, but as we get to higher frequencies, the inductance values will shoot up, thus rendering our coil connections useless. Once we hit 250khz, our inductance value will change enough to render charging too inefficient based on our requirements.

Moving on to figure 13, we have a wide range of current as the coil is rated for operating temperatures between -20 degrees celsius and 120 degrees celsius.

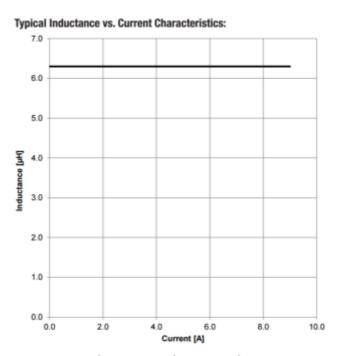


Figure 11: Inductance value according to current

## Typical Inductance vs. Frequency Characteristics:

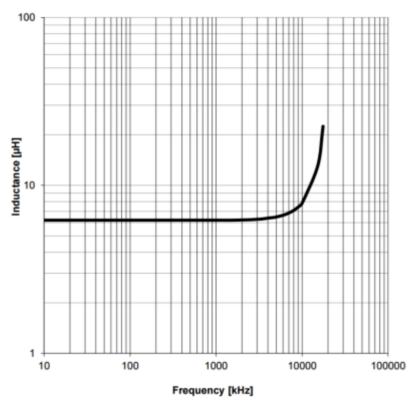


Figure 12: Inductance value according to frequency

# Typical Temperature Rise vs. Current Characteristics:

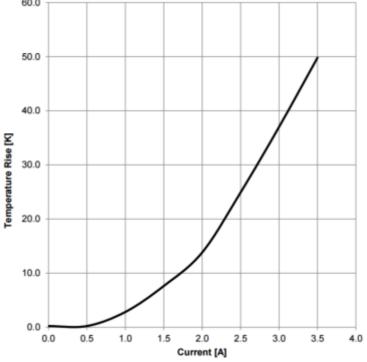


Figure 13: Temperature according to current

## 3. Cost and Schedule

## 3.1 Cost analysis

#### 3.1.1 Labor

We estimated a total of 20 hours of work per week.

| Name                 | Hours invested<br>(hrs) | Hourly rate<br>(\$/hrs) [9] | Salary = hourly rate x<br>hours x 2.5<br>(\$) |
|----------------------|-------------------------|-----------------------------|---|
| Anshil Bhansali      | 200                     | 16                          | \$8,000                                       |
| Brian Slavin         | 200                     | 16                          | \$8,000                                       |
| Jose Javier<br>Rueda | 200                     | 16                          | \$8,000                                       |
| Total                |                         |                             | \$24,000                                      |

**Table 3: Labor costs** 

#### 3.1.2 Parts

#### 3.1.2.1 DC-DC circuit

| Part  | Manufacturer         | Part #           | Description            | Attributes                            | Quantity | Cost(\$) |
|-------|----------------------|------------------|------------------------|---------------------------------------|----------|----------|
| С3    | Taiyo Yuden          | EMK212B7105KG-T  | Capacitor              | Cap=1uF                               | 1        | 0.02     |
| Cff   | Yageo America        | CC0805JRNPO9BN3  | Capacitor              | Cap=39uF                              | 1        | 0.01     |
| Cin   | Vishay-Sprague       | 293D226X9016B2TE | Capacitor              | Cap=22uF,<br>ESR=1.9 Ohm              | 1        | 0.14     |
| Cout  | Vishay-Sprague       | 593D107X0010D2TE | Capacitor              | Cap=100uF,<br>ESR=0.1 Ohm             | 1        | 0.27     |
| Coutx | Kemet                | C0603C105Z8VACTU | Capacitor              | Cap=1uF                               | 1        | 0.01     |
| D1    | ON<br>Semiconductor  | MBRA210LT3G      | Power<br>Rectifier     | VFatIo=0.35V,<br>Io=2A,<br>VRRM=10V   | 1        | 0.16     |
| L1    | Bourns               | SRU8043-150Y     | Inductor               | L=15uH,<br>DCR=0.046 Ohm,<br>IDC = 2A | 1        | 0.33     |
| R1    | Vishay-Dale          | CRCW040249R9FKE  | Resistor               | R=49.9 Ohm                            | 1        | 0.01     |
| Rfbb  | Vishay-Dale          | CRC040249K9FKE   | Resistor               | R=49.9k Ohm                           | 1        | 0.01     |
| Rfbt  | Vishay-Dale          | CRC0402150KFKE   | Resistor               | R=150k Ohm                            | 1        | 0.01     |
| Rt    | Vishay-Dale          | CRC0402392KFKE   | Resistor               | R=392k Ohm                            | 1        | 0.01     |
| U1    | Texas<br>Instruments | LM2621MM/NOPB    | Switching<br>Regulator |                                       | 1        | 0.78     |

**Table 4: DC-DC circuit costs** 

## 3.1.2.2 DC-AC circuit

| Part  | Manufacturer                      | Part #             | Description  | Attributes | Quantity | Cost(\$) |
|---|-----------------------------------|--------------------|--|------------|----------|----------|
| U1  | Texas<br>Instruments              | BQ500511ARHAR      | Low Cost 5V<br>Wireless Power<br>Transmitter<br>Controller |            | 1        | 2.30     |
| U2  | Texas<br>Instruments              | BQ50002ARHBR       | Low Cost 5V<br>Wireless Power<br>Transmitter AFE           |            | 1        | 1.64     |
| L1  | Wurth<br>Elektronik               | 760308111          | Inductor   | 6.3uH      | 1        | 0.05     |
| BUZ1  | TDK                               | PS1240P02CT3       | Buzzer, Piezo,<br>4kHz                                     |            | 1        | 0.3      |
| C1, C2  | Murata                            | GRM188R71E105KA12D | Capacitor  | 1uF        | 2        | 0.15     |
| C3  | Murata                            | GRM188R71A225KE15D | Capacitor  | 2.2uF      | 1        | 0.19     |
| C4, C6  | Murata                            | GRM21BR61E226ME44  | Capacitor  | 22uF       | 2        | 0.26     |
| C5, C7,<br>C11, C20,<br>C22, C23,<br>C24, C27 | TDK                               | C1608X7R1E104K     | Capacitor  | 0.1uF      | 8        | 2.2      |
| C8  | Murata                            | GRM32ER71E226KE15L | Capacitor  | 22uF       | 1        | 0.12     |
| C9, C26                                       | TDK                               | C1608C0G1H102J     | Capacitor  | 1000pF     | 2        | 0.23     |
| C10, C18                                      | TDK                               | C1608X7R1H473K     | Capacitor  | 0.047uF    | 2        | 0.26     |
| C12   | TDK                               | C1608X7R1H223K     | Capacitor  | 0.022uF    | 1        | 0.08     |
| C13   | Murata                            | GRM188R71H222KA01D | Capacitor  | 2200pF     | 1        | 0.08     |
| C14, C16,<br>C17, C19                         | TDK                               | C3216C0G1E104J     | Capacitor  | 0.1uF      | 4        | 0.17     |
| C15   | TDK                               | C1608C0G1H272J     | Capacitor  | 2700pF     | 1        | 0.26     |
| C21   | Murata                            | GRM188R61C225KE15D | Capacitor  | 2.2uF      | 1        | 0.13     |
| C25   | Murata                            | GRM188R71A474KA61D | Capacitor  | 0.47uF     | 1        | 0.03     |
| D1, D6  | Lite-On                           | LTST-C190KGKT      | LED  | Green      | 2        | 0.05     |
| D2, D3  | Micro<br>Commercial<br>Components | MMDL914-TP         | Diode, Switching   | 100V       | 2        | 0.1      |
| D4  | Lite-On                           | LTST-C190KFKT      | LED  | Orange     | 1        | 0.05     |
| D5  | Lite-On                           | LTST-C190CKT       | LED  | Red        | 1        | 0.05     |
| NTC1  | TDK                               | NTCG163JF103F      | Thermistor NTC   | 10k Ohm    | 1        | 0.45     |
| R1  | Susumu Co Ltd                     | RG1608P-1133-B-T5  | Resistor   | 113k Ohm   | 1        | 0.05     |

| R2                           | Yageo America | RT0603BRD077K5L   | Resistor         | 7.5k Ohm     | 1 | 0.07 |
|------------------------------|---------------|-------------------|------------------|--------------|---|------|
| R3, R5                       | Vishay-Dale   | CRCW12060000Z0EA  | Resistor         | 0            | 2 | 0.05 |
| R4, R9,<br>R17, R19          | Vishay-Dale   | CRCW06031K00FKEA  | Resistor         | 1k Ohm       | 4 | 0.31 |
| R6                           | Yageo America | RC0603FR-0769K8L  | Resistor         | 69.8k<br>Ohm | 1 | 0.09 |
| R7, R12,<br>R20, R24,<br>R28 | Yageo America | RC0603FR-0710KL   | Resistor         | 10k Ohm      | 5 | 0.36 |
| R8, R16                      | Panasonic     | ERJ-S6SJR20V      | Resistor         | 0.2 Ohm      | 2 | 0.24 |
| R10                          | Yageo America | RC0603FR-07249KL  | Resistor         | 249k Ohm     | 1 | 0.14 |
| R11                          | Vishay-Dale   | CRCW06032R00FKEA  | Resistor         | 2 Ohm        | 1 | 0.12 |
| R13                          | Susumu Co Ltd | RG1608P-7682-B-T5 | Resistor         | 76.8k<br>Ohm | 1 | 0.04 |
| R14                          | Yageo America | RT0603BRD0710KL   | Resistor         | 10.0k<br>Ohm | 1 | 0.03 |
| R15                          | Yageo America | RC0603JR-0747KL   | Resistor         | 47k Ohm      | 1 | 0.07 |
| R18                          | Ohmite        | LVK12R020DER      | Resistor         | 0.02 Ohm     | 1 | 0.06 |
| R21, R22,<br>R27             | Yageo America | RC0603FR-07100KL  | Resistor         | 100k Ohm     | 3 | 0.27 |
| R23                          | Yageo America | RC0603FR-07200KL  | Resistor         | 200k Ohm     | 1 | 0.1  |
| R25                          | Yageo America | RC0603FR-0724K9L  | Resistor         | 24.9k<br>Ohm | 1 | 0.1  |
| R26                          | Yageo America | RC0603FR-0793K1L  | Resistor         | 93.1k<br>Ohm | 1 | 0.1  |
| C28                          | TDK           | C1608X7R1E104K    | Capacitor        | 0.1uF        | 0 | 0.12 |
| L2                           | Murata        | DLW5BTM102TQ2K    | Coupled Inductor |              | 0 | 2.15 |
|                              |               |                   |                  |              |   |      |

Table 5: DC-AC circuit costs

Total parts cost = \$15.38.

## 3.1.3 Grand Total

| Section | Total       |
|---------|-------------|
| Labor   | \$24,000    |
| Parts   | \$15.38     |
| Total   | \$24,015.38 |

**Table 6: Grand Total costs** 

## 3.2 Schedule

| Week     | Task  | Responsibility  |
|----------|---|-----------------|
| Feb 6    | Write Proposal  | ALL             |
|          | Research options for DC-AC microcontroller                      | Brian           |
|          | Research options for DC-DC microcontroller                      | Javier          |
|          | Prototype, defining the scope of the application                | Anshil          |
| Feb 13   | Design DC-DC converter  | Brian           |
|          | Design DC-AC converter  | Javier & Anshil |
| Feb 20   | Write Design Review   | ALL             |
| Feb 27   | Research options for battery and TX coil                        | Brian           |
|          | Purchase DC-AC and DC-DC components                             | Javier          |
|          | Build user interface with dummy data                            | Anshil          |
| March 6  | Build DC-DC converter   | Brian & Javier  |
|          | Purchase battery and TX coil                                    | Anshil          |
| March 13 | Begin building around DC-AC converter                           | Brian           |
|          | Test DC-DC converter to match requirements                      | Javier          |
|          | Understand communication between the chips and the phone device | Anshil          |
| March 20 | Spring Break: Research  | ALL             |
| March 27 | Test battery separately from other modules                      | Brian           |
|          | Build DC-AC converter   | Javier          |
|          | Test communication chip   | Anshil          |
| April 3  | Test DC-AC converter  | Brian & Javier  |
|          | Develop application   | Anshil          |
| April 10 | Make hardware modifications if necessary                        | Brian           |
|          | Ensure individual module functionality                          | Javier          |
|          | Test app and update if necessary                                | Anshil          |
| April 17 | Prepare Demo  | ALL             |
| April 24 | Write Final Paper   | ALL             |
| May 1    | Finish Final Paper  | Brian           |
|          | Check out lab equipment   | Javier          |
|          | Research market possibilities                                   | Anshil          |

Table 7: Schedule

## 4. Ethics and safety

#### 4.1 Safety statement

When working with electricity it is vital to follow five key safety rules to avoid any injury or harm. First of all, disconnect all voltage sources with the help of fuses or switches. Then, prevent any reconnection by locking out elements and avoiding feedback loops. After this, verify absence of voltage in the installation with voltage detectors. Then, carry out grounding and short-circuiting the active elements of our installation. Finally, provide protection against adjacent live parts by signaling these elements and securing the work zone. [10]

We will follow these rules to make sure that we do not suffer any harm although we will be working with low voltage circuits. We will be especially careful with our capacitors so that they will not discharge instantaneously.

We must be aware that lithium ion batteries are potentially dangerous to the user as well as the environment and should seek out a stable, rechargeable battery solution. By avoiding a lithium metal battery setup, we can produce a more environmentally friendly product since it will be reusable. It's also important to implement safety features into the output portion of the device so we don't run the risk of breaking the consumer's phone.

#### 4.2 Ethics statement

Lithium-ion batteries are difficult to recycle and can be dangerous to the environment if not disposed of properly. Another major concern is the production of the batteries. The mining of lithium contributes to the greenhouse effect, so we must maximize the usage of our battery to avoid endangering our environment as stated in #1 of the IEEE Code of Ethics [11]. Testing battery lifetime and stability will be a major component of our project.

In accordance with #3, we will be honest in stating claims based on data. This implies showing the user the proper data and efficiency of our product. Our system user interface has to be truly honest and show the data collected.

In accordance with #8 and #10 of the IEEE Code of Ethics, we will work all together as a team and we will support our colleagues whenever it is necessary. We reject any form of discrimination. Racism does not belong here at Illinois.

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