

Section (Check One) MWF 10am \_\_\_\_\_ MWF 2pm \_\_\_\_\_

1. \_\_\_\_\_ / 25    2. \_\_\_\_\_ / 25  
 3. \_\_\_\_\_ / 25    4. \_\_\_\_\_ / 25    Total \_\_\_\_\_ / 100

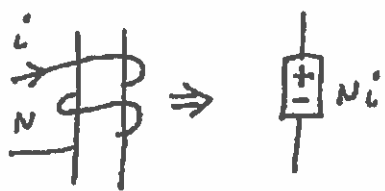
MWF 2pm  
 JTH

Useful information

$\sin(x) = \cos(x - 90^\circ)$      $\vec{V} = \overline{ZI}$      $\vec{S} = \overline{VI}^*$      $\mu_0 = 4\pi \cdot 10^{-7} \text{ H/m}$

$\int_C \mathbf{H} \cdot d\mathbf{l} = \int_S \mathbf{J} \cdot d\mathbf{a}$      $\int_C \mathbf{E} \cdot d\mathbf{l} = -\frac{\partial}{\partial t} \int_S \mathbf{B} \cdot d\mathbf{a}$      $MMF = Ni = \oint \mathfrak{H}$

$\mathfrak{H} = \frac{l}{\mu A}$      $B = \mu H$      $\phi = BA$      $\lambda = N\phi$      $\lambda = Li$  (if linear)



$W_m = \int_0^\lambda i d\hat{\lambda}$      $W_m' = \int_0^i \lambda di$      $W_m + W_m' = \lambda i$      $f^e = \frac{\partial W_m'}{\partial x} = -\frac{\partial W_m}{\partial x}$      $x \rightarrow \theta$

$EFE_{a \rightarrow b} = \int_a^b i d\lambda$      $EFM_{a \rightarrow b} = -\int_a^b f^e dx$      $EFE_{a \rightarrow b} + EFM_{a \rightarrow b} = W_{mb} - W_{ma}$      $\lambda = \frac{\partial W_m'}{\partial i}$      $i = \frac{\partial W_m}{\partial \lambda}$

$f^e \rightarrow T^e$

**Problem 1. (25 points)**

The co-energy of a device is given by

$$W_m'(i, x) = \frac{i^3}{6x} + \frac{i}{x}$$

Find:

- The expression for flux linkage ( $\lambda$ ) as a function of  $i$  and  $x$ . ✓
- The force of electrical origin  $f^e(i, x)$
- The energy stored in the coupling field  $W_m$  as a function of  $i$  and  $x$ .

$$(a) \quad \lambda(i, x) = \frac{\partial W_m'(i, x)}{\partial i} \longrightarrow$$
$$\longrightarrow \lambda(i, x) = \frac{\partial}{\partial i} \left( \frac{i^3}{6x} + \frac{i}{x} \right) = \frac{3i^2}{6x} + \frac{1}{x} = \frac{1}{2} \cdot \frac{i^2}{x} + \frac{1}{x}$$

$$(b) \quad f^e(i, x) = \frac{\partial W_m'(i, x)}{\partial x}$$
$$f^e(i, x) = -\frac{1}{x^2} \left( \frac{i^3}{6} + i \right)$$

$$(c) \quad W_m = \lambda \cdot i - W_m'$$

$$W_m(i, x) = \lambda(i, x) \cdot i - W_m'(i, x)$$
$$= \left( \frac{1}{2} \frac{i^2}{x} + \frac{1}{x} \right) \cdot i - \left( \frac{i^3}{6x} + \frac{i}{x} \right)$$
$$= \frac{i^3}{2x} + \frac{i}{x} - \frac{i^3}{6x} + \frac{i}{x}$$
$$= \frac{2i^3}{6x} = \frac{i^3}{3x}$$

**Problem 2. (25 points)**

An electric machine (1 = stator, 2 = rotor) has the following linear flux linkage vs current characteristic:

$$\lambda_1 = 0.2i_1 + 0.1\sin\theta i_2$$

$$\lambda_2 = 0.1\sin\theta i_1 + 0.3 i_2$$

- What is the energy stored in the coupling field when  $\theta = 90$  degrees,  $i_1 = 3$  Amps, and  $i_2 = 5$  Amps?
- How much energy is given to the coupling field by the mechanical system if  $\theta$  is changed from 90 degrees to 60 degrees while the two currents remain constant?
- How much energy is given to the coupling field by the electrical system during that same path from  $\theta$  equals 90 degrees to 60 degrees while the two currents remain constant?

Since the system is linear,  $W_m = W_m'$ ; thus, I will work with the coenergy to avoid inverting the flux-current relations above.

$$\begin{aligned} a) W_m'(i_1, i_2, \theta) &= \int_0^{i_1} \lambda_1(\tilde{i}_1, 0, \theta) d\tilde{i}_1 + \int_0^{i_2} \lambda_2(i_1, \tilde{i}_2, \theta) d\tilde{i}_2 \\ &= \frac{1}{2} 0.2 i_1^2 + 0.1 \sin\theta \cdot i_1 \cdot i_2 + \frac{1}{2} 0.3 i_2^2 \end{aligned}$$

$$\begin{aligned} W_m'(i_1=3A, i_2=5A, \theta = \frac{\pi}{2}) &= \frac{1}{2} 0.2 \cdot 9 + 0.1 \cdot 1 \cdot 5 \cdot 3 + \frac{1}{2} 0.3 \cdot 25 \\ &= 6.15 \text{ J} = W_m(3A, 5A, \frac{\pi}{2}) \end{aligned}$$

b)  ~~$W_m(3, 5, \frac{\pi}{2}) - W_m(3, 5, \frac{\pi}{3}) = EFC + EFM$~~   
 ~~$= W_m(3, 5, \frac{\pi}{2}) - W_m(3, 5, \frac{\pi}{3})$~~

$$\begin{aligned} EFM_{a \rightarrow b} &= - \int_{\pi/2}^{\pi/3} T^e(i_1=3, i_2=5, \theta) d\theta = - \int_{\pi/2}^{\pi/3} \frac{\partial W_m'(i_1=3, i_2=5, \theta)}{\partial \theta} d\theta \\ &= - \int_{\pi/2}^{\pi/3} 0.1 \cos\theta \cdot 3 \cdot 5 d\theta = -0.1 \cdot 3 \cdot 5 \cdot \sin\theta \Big|_{\pi/2}^{\pi/3} = 0.2 \end{aligned}$$

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$$(c) \quad EFE = \int_{\lambda_1^{(a)}}^{\lambda_1^{(b)}} \underbrace{i_1(\lambda_1, \lambda_2)}_3 d\lambda_1 + \int_{\lambda_2^{(a)}}^{\lambda_2^{(b)}} \underbrace{i_2(\lambda_1, \lambda_2)}_5 d\lambda_2$$
$$= \int_{\cancel{0.2}}^{1.033} 3 d\lambda_1 + \int_{4.5}^{0.26} 5 d\lambda_2 = -0.4 \text{ J}$$

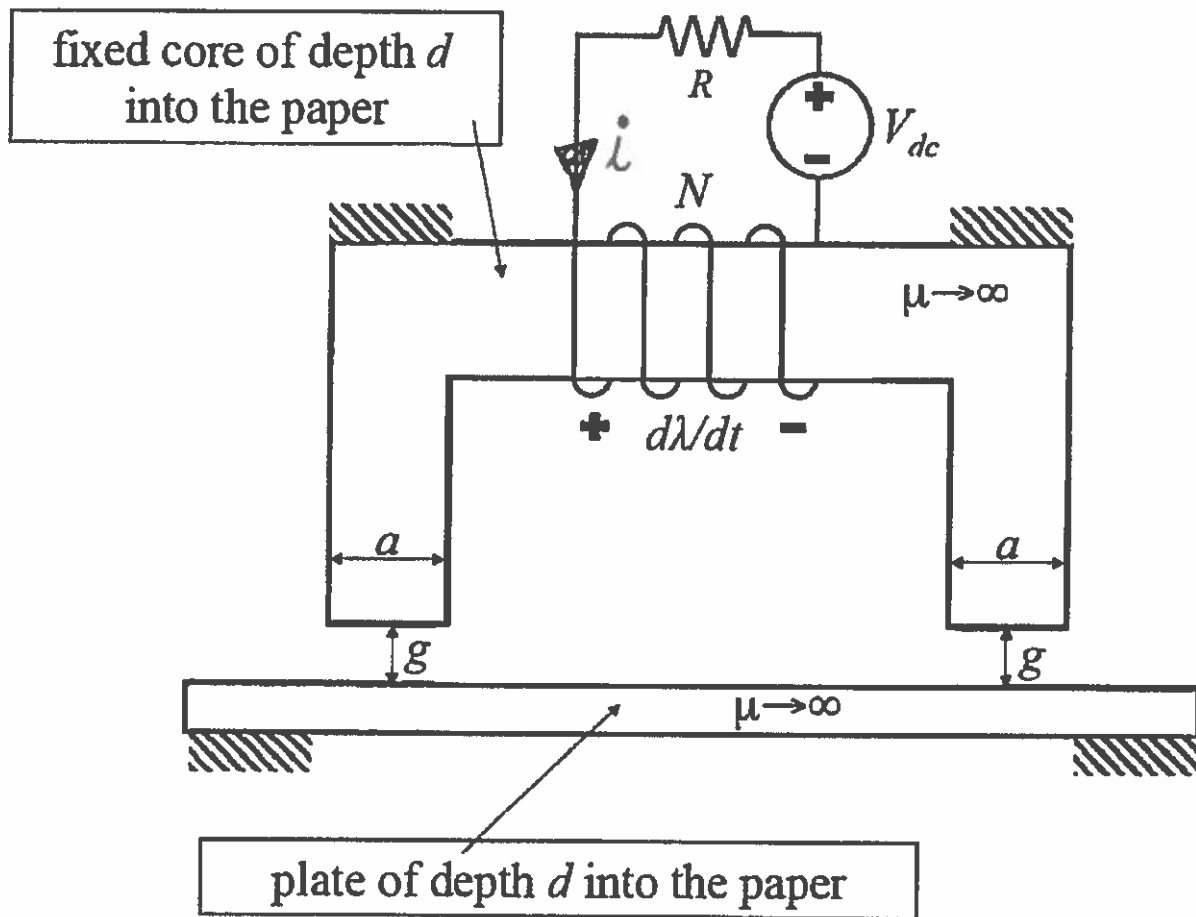
$$\lambda_1^{(a)} = 0.2 \cdot 3 + 0.1 \cdot \sin \frac{\pi}{2} \cdot 5 = 0.6 + 0.5 = 1.1$$

$$\lambda_1^{(b)} = 0.2 \cdot 3 + 0.1 \cdot \sin \frac{\pi}{3} \cdot 5 = 1.033$$

$$\lambda_2^{(a)} = 0.2 \cdot 5 + 0.1 \cdot \sin \frac{\pi}{2} \cdot 5 = 4.5$$

$$\lambda_2^{(b)} = 0.2 \cdot 5 + 0.1 \cdot \sin \frac{\pi}{6} \cdot 5 = 0.26$$

Problem 3. (25 points.)



For the system above, assume that a steady-state operating point has been reached; then:

- a) Find an expression for the flux linkage,  $\lambda$ , that includes  $g$  and  $V_{dc}$ . (6pt)

For the  $i$  in the figure, we have that

$$\lambda(i, g) = \frac{\mu_0 \cdot N^2 \cdot a \cdot d}{2 \cdot g} i$$

$$\text{KVL : } V_{dc} = R \cdot i + \frac{d\lambda}{dt}$$

$$\text{In steady state, } \frac{d\lambda}{dt} = 0 \rightarrow i = \frac{V_{dc}}{R};$$

$$\text{Thus } \lambda(V_{dc}, g) = \frac{\mu_0 N^2 a d}{2g \cdot R} V_{dc}$$

- b) Find an expression for the energy stored in the coupling magnetic field that includes  $g$  and  $V_{dc}$ . (6pt)

From the flux relation  $\lambda(i, g)$  and since the system is linear, we can work with the coenergy:

$$W_m'(i, g) = \int_0^i \frac{\mu_0 N^2 a d}{2g} i \, di = \frac{\mu_0 N^2 a d}{4g} i^2$$

Since  $i = \frac{V_{dc}}{R}$ ,  $W_m'(g, V_{dc}) = \frac{\mu_0 N^2 a d}{4gR^2} V_{dc}^2$

- c) Find an expression for the co-energy that includes  $g$  and  $V_{dc}$ . (6pt)

$$\begin{aligned} W_m'(g, V_{dc}) &= W_m'(g, V_{dc}) \\ &= \frac{\mu_0 N^2 a d}{4gR^2} V_{dc}^2 \end{aligned}$$

- d) Find an expression for the force of electrical origin that tries to reduce the airgap that includes  $g$  and  $V_{dc}$ . (7pt)

$$f^e(i, g) = \frac{\partial W_m'(i, g)}{\partial g} = - \frac{\mu_0 N^2 a d i^2}{4g^2}$$

Again, since  $i = \frac{V_{dc}}{R}$

We have that

$$f^e(V_{dc}, g) = - \frac{\mu_0 N^2 a d}{4g^2 R^2} V_{dc}^2$$

OR could compute magnitude only  
(no minus sign)

**Problem 4. (25 points.)**

The rotor angle dynamics of a synchronous generator are described by the following second-order non-linear differential equation:

$$M \frac{d^2 \delta}{dt^2} + B \frac{d\delta}{dt} = P - K \sin \delta,$$

where  $M$ ,  $B$ ,  $P$ , and  $K$  are positive constants.

- a) If you were to write the above differential equation in state-space form, which variables would you take as states? (5pt)

$$\begin{cases} X_1 := \delta \\ X_2 := \frac{d\delta}{dt} \end{cases} \rightarrow X = [X_1, X_2]^T$$

- b) For the states you chose in a), write the state-space model equations. (10pt)

$$\frac{dx_1}{dt} = \frac{d\delta}{dt} = X_2 \rightarrow \boxed{\frac{dx_1}{dt} = X_2}$$

$$\frac{dx_2}{dt} = \frac{d^2\delta}{dt^2} = \frac{1}{M} \left( P - K \sin \delta - B \frac{d\delta}{dt} \right) \rightarrow$$

$$\rightarrow \boxed{\frac{dx_2}{dt} = -\frac{B}{M} X_2 + \frac{1}{M} (P - K \sin X_1)}$$

- c) Find the equilibrium points of the state-space model in b) that correspond to values of  $\delta$  between  $0$  and  $\pi$ . (10pt)

Eq. points:

$$\frac{dx_1}{dt} = 0 \Rightarrow X_2^{eq} = 0$$

$$\frac{dx_2}{dt} = 0 \rightarrow 0 = -\frac{B}{M} X_2^{eq} + \frac{1}{M} (P - K \sin X_1) \Rightarrow$$

$$X_1^{eq(1)} = \arcsin \left( \frac{P}{K} \right) \rightarrow$$

$$X_1^{eq(2)} = \pi - \arcsin \left( \frac{P}{K} \right)$$

