

ECE 430 Exam #2, Spring 2009  
90 Minutes

Name: Solution

Section (Check One) MWF \_\_\_\_\_ TTH \_\_\_\_\_

1. \_\_\_\_\_ / 25    2. \_\_\_\_\_ / 25

3. \_\_\_\_\_ / 25    4. \_\_\_\_\_ / 25    Total \_\_\_\_\_ / 100

Useful information

$$\mu_0 = 4\pi \cdot 10^{-7} \text{ H/m}$$

$$\int_C \mathbf{H} \cdot d\mathbf{l} = \int_S \mathbf{J} \cdot \mathbf{n} da$$

$$\int_C \mathbf{E} \cdot d\mathbf{l} = -\frac{\partial}{\partial t} \int_S \mathbf{B} \cdot \mathbf{n} da$$

$$\mathfrak{R} = \frac{l}{\mu A} \quad MMF = Ni = \phi \mathfrak{R} \quad B = \mu H \quad \phi = BA \quad \lambda = N\phi \quad \lambda = Li \text{ (if linear)}$$

$$W_m = \int_0^\lambda i d\hat{\lambda} \quad W_m' = \int_0^i \lambda d\hat{i} \quad W_m + W_m' = \lambda i \quad f^e = \frac{\partial W_m'}{\partial x} = -\frac{\partial W_m}{\partial x} \quad x \rightarrow \theta$$

$$\frac{EFE}{a \rightarrow b} = \int_a^b i d\lambda \quad \frac{EFM}{a \rightarrow b} = -\int_a^b f^e dx \quad \frac{EFE}{a \rightarrow b} + \frac{EFM}{a \rightarrow b} = W_{mb} - W_{ma} \quad \lambda = \frac{\partial W_m'}{\partial i} \quad i = \frac{\partial W_m}{\partial \lambda}$$

1. (25 points)

A 2-phase machine, with two stator coils and one rotor coil, has following flux linkage-current relationship

$$\begin{bmatrix} \lambda_{sa} \\ \lambda_{sb} \\ \lambda_r \end{bmatrix} = \begin{bmatrix} L_s & 0 & M \cos \theta \\ 0 & L_s & M \sin \theta \\ M \cos \theta & M \sin \theta & L_r \end{bmatrix} \times \begin{bmatrix} i_{sa} \\ i_{sb} \\ i_r \end{bmatrix}$$

- a) Compute the co-energy  $W'_m$  (10 points)  
 b) Compute the energy  $W_m$  (5 points)  
 c) Find the torque of electrical origin  $T^e$  (10 points)

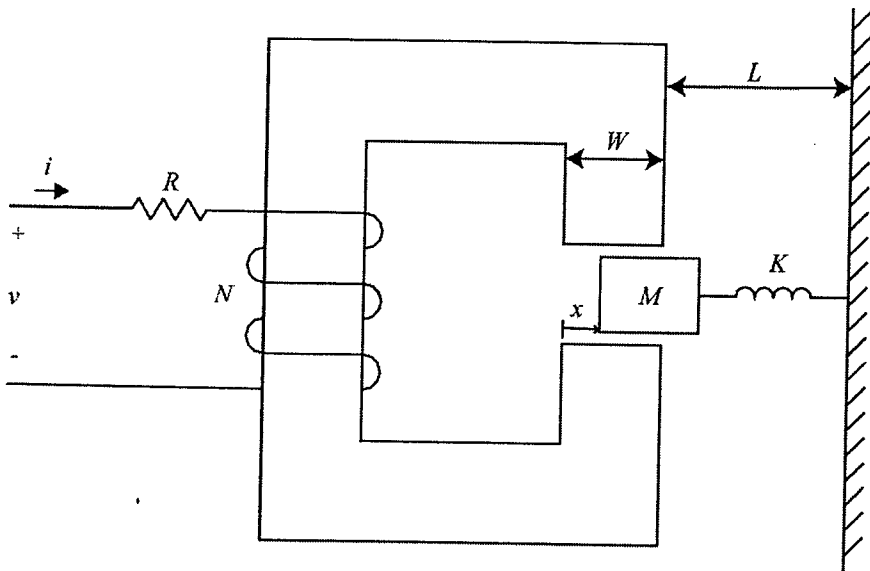
a)  $W'_m = \frac{1}{2} L_s i_{sa}^2 + \frac{1}{2} L_s i_{sb}^2 + M \cos \theta i_{sa} i_r + M \sin \theta i_{sb} i_r + \frac{1}{2} L_r i_r^2$

b)  $W_m = W'_m =$  // (linear system)

c)  $T^e = \frac{\partial W'_m}{\partial \theta} = -M \sin \theta i_{sa} i_r + M \cos \theta i_{sb} i_r \text{ NM}$

2. (25 points)

The figure below shows a magnetic structure composed of an iron core and a moveable iron plunger. The plunger is connected to a solid structure through a spring with stiffness coefficient  $K$ . The spring exerts no force when the plunger is located at  $x = C$ . The plunger is separated from the core by a constant gap of length  $g$  above and below the plunger. The horizontal length of the plunger is  $W$ . The plunger and the core both have a depth of  $D$ . The iron core and plunger both have infinite permeability. You should neglect fringing in the air gaps. You may neglect the force of gravity and all friction.



Depth:  $D$   
 $\mu \rightarrow \infty$

$$v = iR + \frac{d\lambda}{dt}$$

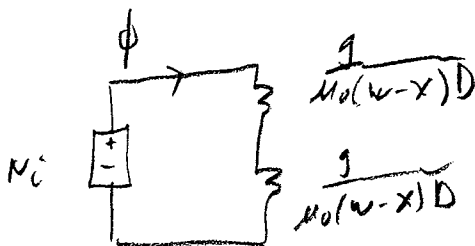
$$\lambda = L(x)i$$

$$v = \frac{dx}{dt}$$

$$m \frac{dv}{dt} = -k(x-c) + f^e$$

For  $v = d\lambda/dt$ ,

- Find the flux linkage  $\lambda$  in terms of current  $i$  and position  $x$  plus  $\mu_0$ ,  $N$ ,  $W$ ,  $g$ , and  $D$ .
- Find the force of electric origin either in terms of flux linkage  $\lambda$  and position  $x$ , or in terms of current  $i$  and position  $x$  (whichever you prefer).
- Select either flux linkage  $\lambda$  or current  $i$  as an independent state and write the three differential equations that describe all of the dynamics of this electromechanical system with voltage  $v$  as the only input.



$$\lambda = N\phi = \frac{N^2 i^2}{\frac{2g}{\mu_0(w-x)D}} = \frac{N^2 \mu_0 (w-x) D}{2g} i^2$$

$$W_m^i = \frac{N^2 \mu_0 (w-x) D}{4g} i^2$$

$$f^e = -\frac{N^2 \mu_0 D}{4g} i^2$$

(this page is extra space for showing work)

$$v = cR + \frac{N^2 \mu_0 (w-x) D di}{2g} \frac{d}{dt} - \frac{N^2 \mu_0 D i v}{2g}$$

$$\frac{dx}{dt} = v$$

$$m \frac{dv}{dt} = -k(x-c) - \frac{N^2 \mu_0 i^2 D}{4g}$$

OR

$$v = \frac{2g \lambda R}{N^2 \mu_0 (w-x) D} + \frac{d\lambda}{dt}$$

$$\frac{dx}{dt} = v$$

$$m \frac{dv}{dt} = -k(x-c) - \frac{N^2 \mu_0 D}{4g} \left( \frac{2g \lambda}{D N^2 \mu_0 (w-x)} \right)^2$$
$$= -k(x-c) - \frac{g \lambda^2}{D N^2 \mu_0 (w-x)^2}$$

3. (25 points)

The co-energy of a device is given by

$$W_m'(i, x) = \frac{i^5}{24x} + \frac{i^3}{6x} + \frac{i}{x}$$

$$\lambda = \frac{5i^4}{24x} + \frac{3i^2}{6x} + \frac{1}{x}$$

Find:

- The force of electrical origin  $f^e(i, x)$
- The energy stored in the coupling field  $W_m$  as a function of  $i$  and  $x$ .

$$a) \quad f^e = -\frac{i^5}{24x^2} - \frac{i^3}{6x^2} - \frac{i}{x^2}$$

$$b) \quad W_m = \lambda i - W_m' = \frac{5i^5}{24x} + \frac{3i^3}{6x} + \frac{i}{x} - \frac{i^5}{24x} - \frac{i^3}{6x} - \frac{i}{x}$$

$$= \frac{4i^5}{24x} + \frac{2i^3}{6x} = \frac{i^5}{6x} + \frac{i^3}{3x}$$

4. (25 points)

An electromechanical system has a nonlinear flux linkage-current relationship:

$$i = \frac{\lambda^2}{x}$$

- Find the energy stored in the coupling field when  $i = 2.0$  Amps,  $x = 0.02$  m,  $\lambda = 0.2$  WbTn
- Find the force of electric origin when  $i = 2.0$  Amps,  $x = 0.02$  m,  $\lambda = 0.2$  WbTn
- Find the energy transferred from the mechanical system into the coupling field (EFM) as the position  $x$  changes from  $0.02$  m to  $0.01$  m along a constant flux linkage ( $0.2$  WbTn) path.

$$a) \quad w_m = \int_0^{\lambda} i \, d\lambda = \frac{\lambda^3}{3x}$$

$x = \text{const}$

$$w_m \Big|_{x=0.02} = \frac{.2^3}{3 \times .02} = \frac{.008}{.06}$$

$$\lambda = .2 \quad \Rightarrow \quad \frac{8}{60} \text{ J}$$

$$b) \quad f^e = - \left( - \frac{\lambda^3}{3x^2} \right) = \frac{\lambda^3}{3x^2}$$

$$f^e \Big|_{x=0.02} = \frac{.2^3}{3 \times .02^2} = \frac{.008}{3 \times .0004}$$

6.66

$$\lambda = .2 \quad \Rightarrow \quad \frac{80}{3} = \frac{20}{3} \text{ N}$$

$$c) \quad \text{EFM}_{a \rightarrow b} = \int_{.02}^{.01} -f^e \, dx = - \left( - \frac{\lambda^3}{3x} \right) \Big|_{x=.02}^{x=.01} = \frac{.2^3}{3 \times .01} - \frac{.2^3}{3 \times .02}$$

$$= \frac{.008}{.03} - \frac{.008}{.06} = \frac{8}{30} - \frac{8}{60} \text{ J}$$

0.133